

ADA067738

DUE FILE COPY

LÉVELS

VRL Memorandum Report 5959 NASA CR-152,222

Final Technical Report
Part I, Gallium-Doped Germanium



Evaluation of Photoconductors

W. J. MOORE

Semiconductors Branch
Electronics Technology Division

April 12, 1979



NASA Contract RA 60085-



NAVAL, RESEARCH LABORATORY Westington, D.C.

المعاطعة وبالمعادلة ومناهأ بالخدرات استعبار

79 04 20 028

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered) READ INSTRUCTIONS BEFORE COMPLETING FORM REPORT DOCUMENTATION PAGE 2. GOVT ACCESSION NO. 3. RECIPIENT'S CATALOG NUMBER NRL Memorandum Report 3939 NASA CR-152,222 s. Type of REPORT & PERIOD COVERED Final Report covering period 4. TITLE (and Subtitle) FINAL TECHNICAL REPORT - PART I, GALLIUM-DOPED Dec. 1976 to Sept. 1978 GERMANIUM - EVALUATION OF PHOTOCONDUCTORS PERFORMING ORG. REPORT NUMBER CONTRACT OR GRANT NUMBER(s) NASA-RA-32035-B W. J. Moore PERFORMING ORGANIZATION NAME AND ADDRESS PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS Naval Research Laboratory NRL Problem R18-02 Washington, D.C. 20375 Program Element 0 Project RA 32035-B II. CONTROLLING OFFICE NAME AND ADDRESS 12. REPORT DATE April 12, 1979 Naval Research Laboratory 13. NUMBER OF PAGES Washington, D.C. 20375 55 15. SECURITY CLASS. (of this report) UNCLASSIFIED 15a. DECLASSIFICATION/DOWNGRADING 16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited. 17. DISTRIBUTION STATEMENT (of the obstract entered in Block 20, if different from R Evaluation of Photoconductors, wrt I. Gallium - Doped Germanius Far infrared detectors Gallium-doped germanium TRACT (Continue on reverse side if necessary and identify by block nu Gallium-doped germanium far infrared detectors manufactured by the Santa Barbara Research Center under NASA Contract have been evaluated at low temperatures and low background simulating the space environment. Signal and noise characteristics have been determined for detector temperatures in the 2K to 4K range. Optimum performance occurs at about 2.5K for all devices tested. The minimum average NEP in the 40-130 micron region has been found to be approximately 4×10^{-17} watt Hz^{-1/2} at a frequency of 1 Hz. 54x 10 to The - 17th gower watt/sq noot DD , FORM 1473 EDITION OF ! HOV 65 IS OBSOLE S/N 0102-014-6601

The state of

FINAL TECHNICAL REPORT PART I, GALLIUM-DOPED GERMANIUM Evaluation of Photoconductors

PSTIFICATION BISTINGTH WITH CENCE AVAILABILITY CENCE AVAILABILI

Introduction

An extended program has been carried out to determine the characteristics of gallium-doped germanium detectors produced by the Santa parbara Research Center. Particular attention has been paid to those characteristics which were believed to be unusual or otherwise of an unpredictable nature with respect to IRAS performance.

Some general conclusions are possible based on these tests and, although many are self-evident, they will be repeated here.

- (1) These devices can operate in the background limited (BLIP) condition for backgrounds in the 6-7 x 10^8 phot $\sec^{-1} \text{cm}^{-2}$ range (or perhaps lower) at a temperature of 2.5K. Under these conditions the NEP is of the order of $4\text{x}10^{-17}$ watt $\text{Hz}^{-\frac{1}{2}}$.
- (2) Operation at 3K imposes a severe penalty in that it produces conditions equivalent to a background of approximately 2×10^{10} photons $\sec^{-1} \text{cm}^{-2}$ and may increase the 1/f noise above thermal g-r noise. At 3K the NEP is limited to about 1.5×10^{-16} watt $\text{Hz}^{-\frac{1}{2}}$.
- (3) Anomalous signal and noise characteristics were observed with some, but not all, detectors. These anomalies are most severe at the lowest temperatures used in these tests (i.e. 2K). The device exhibiting the greatest anomalies would have optimum performance between 3K and 2K.
 - (4) Cosmic ray pulse fall times observed on both the 3- and 4-

series of detectors were of the order of 2 msec with a transimpedance amplifier and these observed times were amplifier limited.

- (5) Noise spectra increase approximately as $P_n \propto f^{-1}$, where P_n is the noise power and f is the frequency, from 1 Hz down to at least .03 Hz.
- (6) Signal responsivities were in excellent agreement with the manufacturer's data. Variations from the manufacturer's data occurred only as a result of differences in the operating conditions here and at SBRC. In general, a device would have substantially higher resistance at a given temperature and background in these tests than indicated by the manufacturer. 1
- (7) The responsivity of these devices was high. Scaling previous Ge:Ga data calculated by the "power inband" method to the dimensions of these devices (a factor of 170) predicts responsivities of the order of 180 mho watt⁻¹; whereas maximum measured responsivities for these devices were greater than 200 mho watt⁻¹. It is concluded that the material from which these devices were constructed is at least as good as the best NRL material and that no serious damage occurs in processing.
- (8) Signal vs frequency data determined from device response to a signal step indicate rolloff due to a single 6 dB/octave rolloff with a 3 dB point in the 1-3 Hz range at 3K. Some reduction in 3 dB frequency to about 0.2 to 1 Hz occurs at 2.5K. At 2K a second, slower, time constant appears and introduces additional signal reduction.
- (9) Interfacing these devices to preamplifiers presents significant problems. These devices will have resistances of the order of $1x10^{12}$ ohms at minimum background (\emptyset \sim $5x10^8$ phot sec⁻¹) at 2.5K and consider-

ably lower resistance at higher backgrounds and higher temperature.

As a result it is difficult to interface these devices optimally to transimpedance amplifiers for all possible operating conditions. This has been a substantial problem in these tests.

Experimental Details and Results

A. Signal and NEF Measurements

The requirements of these tests (low background, low temperature) necessitated the design and construction of the third calibration system to be used in this series of tests. This system is based on the dipstick system built by the author at Cornell University. The major changes from the Cornell system were an increase in the dipstick diameter and inclusion of a movable aperture block which served as a low speed chopper for frequencies at or below 1Hz. The design of this system is shown in Fig. 1. Results reported here will not include data on sample 3- 2b1-4 which was measured early in the program nor will the details of the anomalous signal response with time at 2K be reviewed. Both these topics were covered in interim reports. A typical calibration run consisted of strip chart recordings of the output of the source-follower preamplifier for bias off, bias on-signal off, and bias on-signal on. These measurements were repeated for various values of bias and as a function of both blackbody and detector temperatures. Results are presented in Appendix A.

The data in Appendix A include a number of entries for each calibration condition. These entries are described below.

TEMP. = The detector temperature as determined by a carbon resistor

on the detector mounting block. The entire enclosure was flooded with He gas for thermal equilibrium with the bath.

BB INTEGRATED FROM ... TO ...

All responsivities (both power and photon) were calculated using all blackbody power in the approximate spectral band of the detector with cold crystal sapphire and crystal quartz filters.

BB TEMP = The temperature of the calibration blackbody as measured with a type E thermocouple. Both room temperature and liquid nitrogen temperature reference junctions were used during this study.

BIAS = The applied bias across the detector plus load.

BIAS DELTA V = The change in output of the source-follower preamplifier for a change from bias-off to bias-on. This value is the potential drop across the detector times the preamplifier gain. The preamplifier gain was approximately 0.9.

SIG DEL V = The change in source-follower output for a change from signal radiation off to signal on. Signal radiation was turned off with the movable shutter.

DC/1 Hz = This ratio is the ratio of peak dc signal volts to peak-topeak signal volts when chopping with the movable shutter at 1 Hz.

NOISE = The rms noise value observed on a wave analyzer at 1 Hz.

BLACKBODY OUTPUT = The calculated blackbody radiation incident on the detector-sensitive area for the temperature and integration band given.

SIG. CONDUCTANCE (DC) = This is a derived quantity equal to the change in conductance per watt (or photon per sec) of signal. The calculation uses the large signal equations to derive a number characteristic of the device which is relatively independent of bias and measurement

conditions.

VOLT. RESP. (DC) ≡ The voltage responsivity calculated with the largesignal equations. When the signal is, in fact, large the calculation
determines the correct small-signal responsivity.

CURR. RESP. (DC) = The current responsivity.

SIG. CONDUCTANCE (1 Hz) = As above but calculated using the 1 Hz signal as determined from the DC/1 Hz ratio.

VOLT. RESP. (1 Hz) = As above for 1 Hz.

CURR. RESP. (1 Hz) = As above for 1 Hz.

DETECTOR RESISTANCE = The resistance of the detector as calculated from the values of total bias, bias across detector, and load resistance.

The major uncertainty is in the load resistance. An error as great as 40% is possible. Note that the SBRC data sheets assume a load resistance independent of temperature below 3K. An error in excess of 100% is possible with that assumption.

DETECTOR BIAS = A number equal to the bias delta V divided by preamp gain.

BACKGROUND PHOTON FLUX DENSITY = The photon flux density required to produce the measured detector resistance calculated using the measured signal conductance. Note that the value calculated assumes that the detector resistance is optically (not thermally) limited. For a thermally limited resistance the background can be considered to be an optical equivalent of the operating temperature.

PC GAIN (Q.E. = 0.3) ≡ This quantity (and the following quantities) are calculated using both the ac and dc responsivities described above with an assumed quantum efficiency of 0.3. Calculation of device parameters

using the ac responsivity implies that the lower ac response is the result of a slow process within the detector and not a result of RC rolloff prior to the preamp. A comparison of experimental NEP data with theoretical BLIP NEP values indicates that the ac results are appropriate for a detector at 2.5K (i.e. slow processes within the detector dominate the signal rolloff at 2.5K) while the dc results apply at 3K (i.e. RC rolloff dominates the signal rolloff at 3K).

SHOT NOISE = A calculated shot noise assuming a quantum efficiency of 0.3.

BLIP NEP = A calculated NEP for a noise equal to the shot noise.

QUAN EFFIC. IF BLIP = The quantum efficiency required to make the measured NEP a background limited value. When this quantity is of the order of 0.3 one can consider the detector to be, in fact, BLIP. Some of the NEP data is shown graphically in Figs. 2, 3 and 4.

Signal vs frequency measurements were made by determining the response to a step increase in signal. Analysis of these signal steps indicated a predominantly one time constant rise for operating temperatures of 2.5K or greater. At 2.5K the time constant ranged from 0.1 to 0.8 seconds and decreased to approximately .05 sec at 3K. Very slow secondary time constants were observed at 2K where T $^{\sim}$ 6 sec. These rise times indicate 3 dB frequencies at 3Hz for 3K operation and from 0.2 to 1 Hz for 2.5K operation.

B. Spectral Response

Spectral response has been determined by two different experimental techniques. Initial measurements were made with a grating spectrometer

and a Golay cell. These measurements indicated relatively little reduction in response at 50 microns with respect to the peak response near 100 microns. However, these measurements were considered to be of questionable value due to contamination of the spectrometer output by higher order radiation in spite of a considerable effort to minimize out of band signals.

In order to avoid these problems a new approach was taken. Detector signal measurements were made as a function of blackbody temperature over the 30K to 120K range. An assumed detector response was then fed to a desktop computer which calculated and plotted the responsivity (mho phot⁻¹ sec) for each temperature. The spectral response was varied to give the most consistent responsivity over the blackbody temperature range used. This technique is not sensitive to details in the spectral response curve but does not have serious out-of-band radiation problems. The major weakness of this method is contamination by light leaks around the blackbody. These tend to cause an underestimation of the short wavelength response and therefore result in a worst case spectrum. Short wavelength response will be at least as good as indicated from these measurements.

A series of plots for two detectors are given in Figs. 5 through

14. The detector (with quartz and sapphire filters) is assumed to turn
on at Ll microns, the smallest sensitive wavelength, rise linearly to

L2 microns and fall to zero at L3 microns. The relative response at

L1 is given by G1. The average conductance responsivity is given by

G. An inset shows the assumed spectral response.

C. Noise vs Frequency

As originally envisioned the noise vs frequency measurements below 1 Hz would have been done with an analog-to-digital converter and a computer. Equipment malfunctions prevented the use of this technique and forced reliance on an analog approach. This limited the lowest frequency at which we could make measurements to .03 Hz rather than the planned .01 Hz but did pay a dividend by making apparent a possible problem with digital noise data.

Detectors of the size of the SBRC Ge:Ga devices (.05 x .15 x .3 cm) exhibit a cosmic ray noise pulse every few minutes at sea level. Digital noise data consists of many digitized samples taken from the noise waveform over several minutes. In order to prevent aliasing of the Fourier transform a high frequency cutoff filter limits the maximum frequency present to half the inverse of the sampling period. That is $f_{max} = \frac{1}{2T}$, where T is the sampling period. Therefore at least two samples are taken per period of the highest frequency present. A cosmic ray pulse passing through such filters is considerably reduced in amplitude and broadened but not eliminated. These pulses then contribute to the measured noise at low frequencies.

The analog system used here consists of an FM analog tape recorder on which the noise is recorded at minimum tape speed (1 7/8 ips) and played back at maximum tape speed (60 ips) resulting in a frequency multiplication by a factor of 32. On playback the noise is measured with a wave analyzer down to 1 Hz. With this system the cosmic ray pulses are very apparent and contribute to the noise spectrum if the result is read on the meter. This problem was avoided by recording the

wave analyzer output on a strip chart recorder and reading between the pulses.

The results on two detectors indicate that the noise increases approximately as 1/f below 1 Hz for the conditions of the tests. These conditions were not optimum for sample Ge:Ga 4-5bl-1 in that the background was higher than desired, and the noise was masked by pulses for f > 0.1 Hz. The data are given in Fig. 15. However, for sample 3-2bl-3 the conditions were nearly optimum ($\phi > 5 \times 10^8$ phot sec⁻¹ cm⁻²). These data are given in Fig. 16.

The noise spectrum for sample 3-2bl-3 is an interesting one in that it appears to consist of a section of noise above about 1 Hz which has been rolled off by the RC time constant and a section of 1/f noise below 1 Hz which is free of RC rolloff. This interpretation is consistent with the observation that this device appears to be nearly BLIP at 1 Hz under these conditions. Above about 2 Hz the device is amplifier noise limited. It is concluded from these spectra that the device noise has a 1/f spectrum throughout the region below 1 Hz.

REFERENCES

- P.R. Bratt and N.N. Lewis, "Development of Doped Germanium Photoconductors for Astronomical Observations at Wavelengths from 30 to 120 Micrometers," Final Technical Report, Contract NAS 2-9385, Santa Barbara Research Center, 30 Nov. 1977 (NASA-CR-152,046).
- W.J. Moore, "100 Micron Detector Development Program" Report No. CRSR 642, Cornell University (1976).

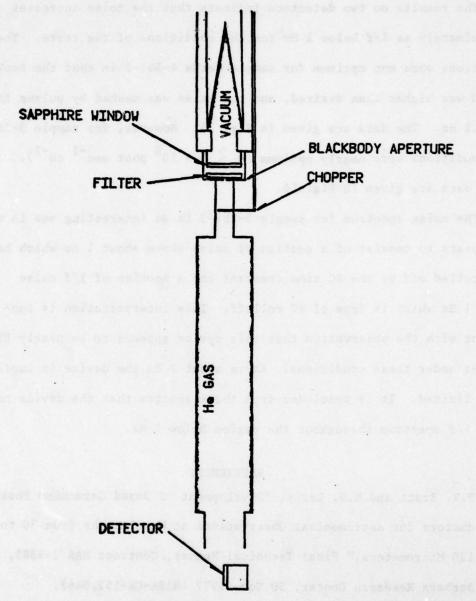


Fig. 1 — A schematic drawing of the calibration apparatus. The calibrating source, a blackbody, is located in vacuum in the upper part of the drawing. A sapphire window separates the blackbody vacuum from the detector atmosphere: low pressure helium gas. A quartz filter, aperture, and manually operated chopper complete the optical components. The assembly is immersed in pumped liquid He for cooling. Temperatures are determined by a type E thermocouple in the blackbody and a carbon resistor on the sample mounting block.

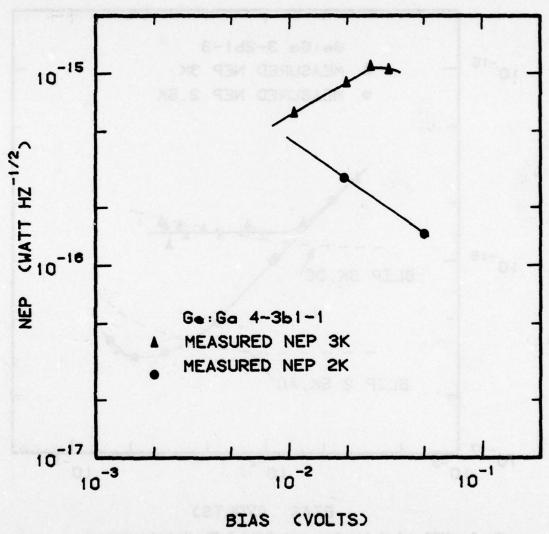


Fig. 2 — NEP at 1 Hz vs bias for sample 4-3bl-1. The anomalous rising curve at 3K was due to excess noise at that temperature attributable to a noisy contact. This noise was absent at 2K but a slow signal response time limited the NEP at that temperature.

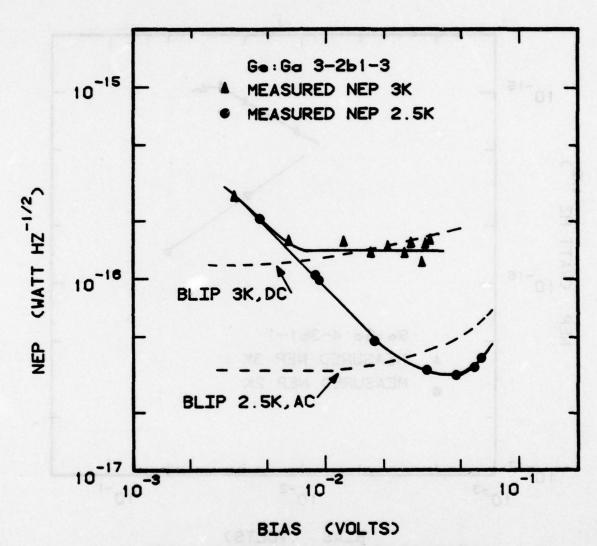


Fig. 3 — NEP at 1 Hz bias for sample 3-2b1-3. The dashed curves are calculated values for the BLIP NEP as discussed in the text.

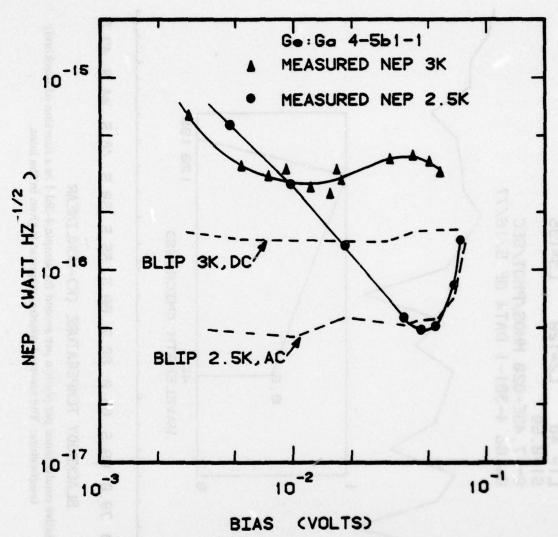


Fig. 4 — NEP at 1 Hz vs bias for sample 4-5b1-1. The dashed curves are calculated values for the BLIP NEP as discussed in the text.

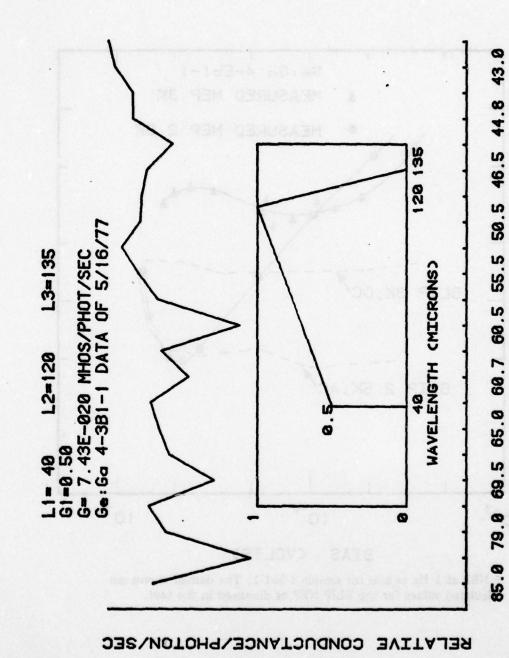
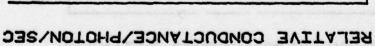
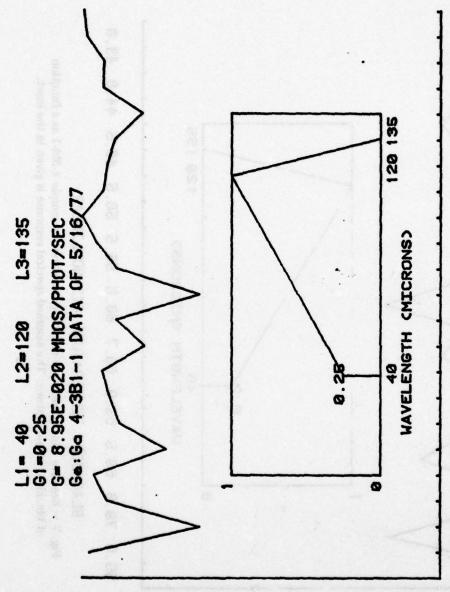


Fig. 5 - Relative conductance per photon per second for sample 4-3bl-1 as a function of blackbody temperature. The assumed spectral response is given in the inset. BLACKBODY TEMPERATURE (K)-NONLINEAR





85.0 79.0 69.5 65.0 60.7 60.5 55.5 50.5 46.5 44.8 43.0 BLACKBODY TEMPERATURE CK3-NONLINEAR

Fig. 6 — Relative conductance per photon per second for sample 4-3bl-1 as a function of blackbody temperature. The assumed spectral response is given in the inset.

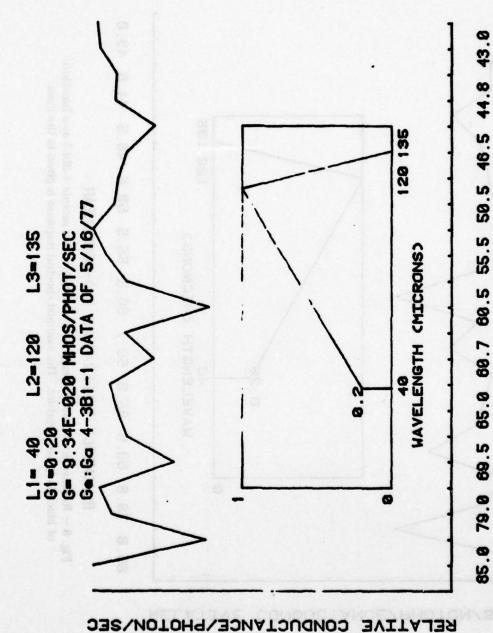


Fig. 7 — Relative conductance per photon per second for sample 4-3bl-1 as a function of blackbody temperature. The assumed spectral response is given in the inset. BLACKBODY TEMPERATURE CKY-NONLINEAR

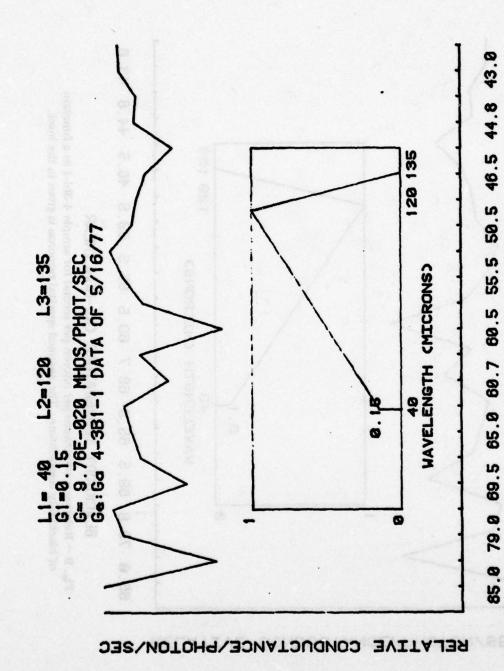


Fig. 8 - Relative conductance per photon per second for sample 4-3bl-1 as a function of blackbody temperature. The assumed spectral response is given in the inset. BLACKBODY TEMPERATURE (K)-NONLINEAR

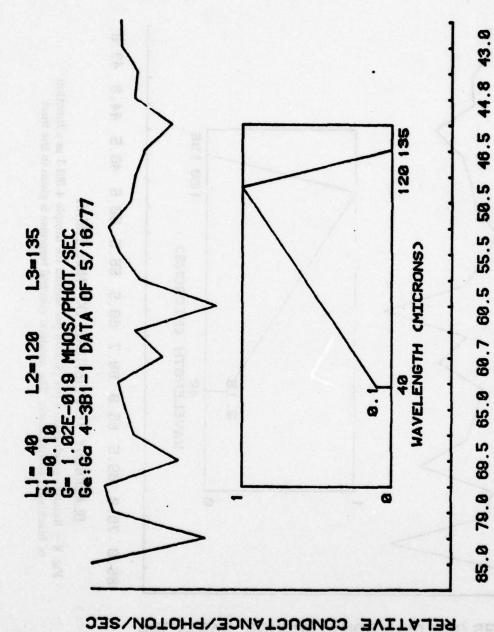
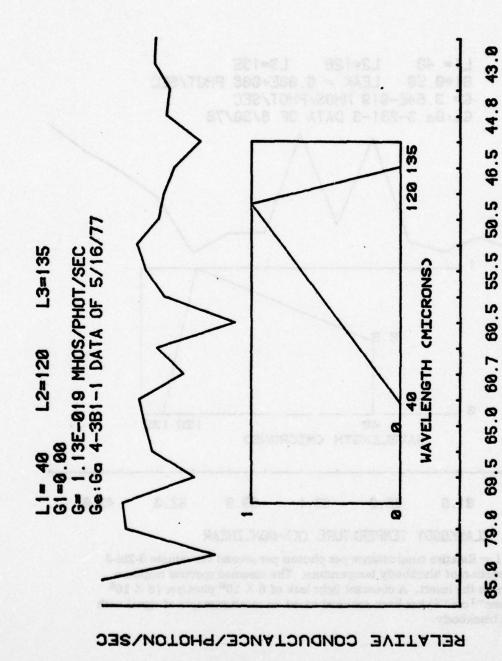


Fig. 9 - Relative conductance per photon per second for sample 4-3bl-1 as a function BLACKBODY TEMPERATURE CK)-NONLINEAR

of blackbody temperature. The assumed spectral response is given in the inset.



BLACKBODY TEMPERATURE (K)-NONLINEAR

Fig. 10 — Relative conductance per photon per second for sample 4-3bl-1 as a function of blackbody temperature. The assumed spectral response is given in the inset.

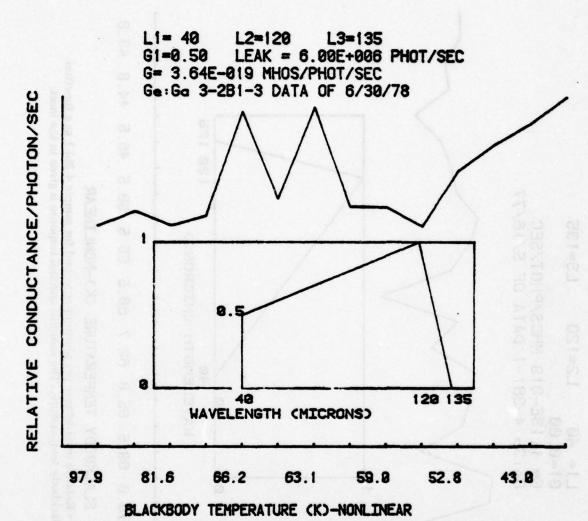


Fig. 11 — Relative conductance per photon per second for sample 3-2bl-3 as a function of blackbody temperature. The assumed spectral response is given in the insert. A constant light leak of 6×10^6 phot/sec (8×10^8) phot $\sec^{-1} \mbox{cm}^{-2}$) has been assumed based on measurements of signal with a cold blackbody.

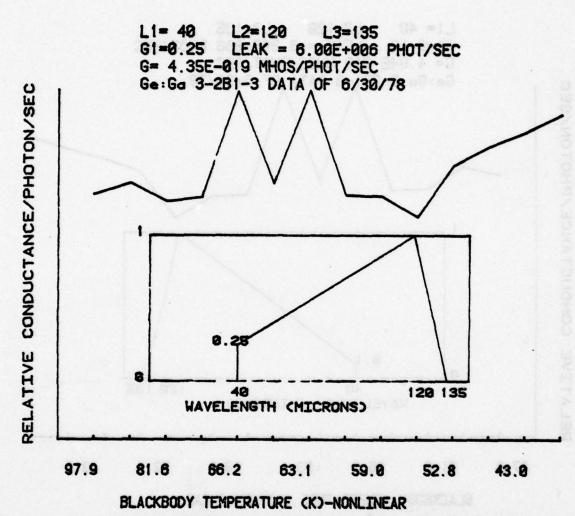


Fig. 12 — Relative conductance per photon per second for sample 3-2bl-3 as a function of blackbody temperature. The assumed spectral response is given in the insert. A constant light leak of 6×10^6 phot/sec (8×10^8) phot sec⁻¹ cm⁻² has been assumed based on measurements of signal with a cold blackbody.

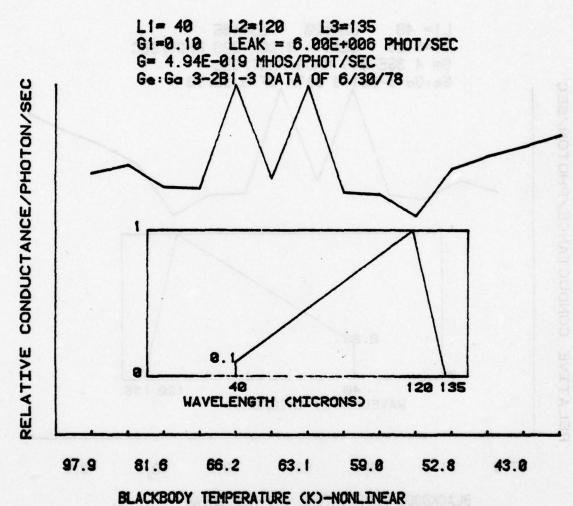
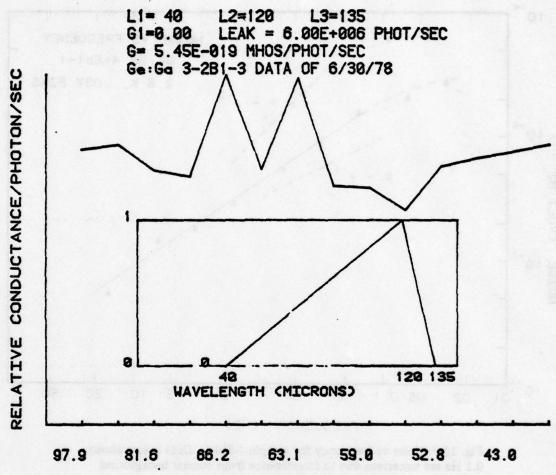


Fig. 13 — Relative conductance per photon per second for sample 3-2bl-3 as a function of blackbody temperature. The assumed spectral response is given in the insert. A constant light leak of 6×10^6 phot/sec (8×10^8) phot sec⁻¹ cm⁻² has been assumed based on measurements of signal

with a cold blackbody.



BLACKBODY TEMPERATURE (K)-NONLINEAR

Fig. 14 — Relative conductance per photon per second for sample 3-2bl-3 as a function of blackbody temperature. The assumed spectral response is given in the insert. A constant light leak of 6×10^6 phot/sec $(8\times10^8$ phot sec⁻¹ cm⁻²) has been assumed based on measurements of signal with a cold blackbody.

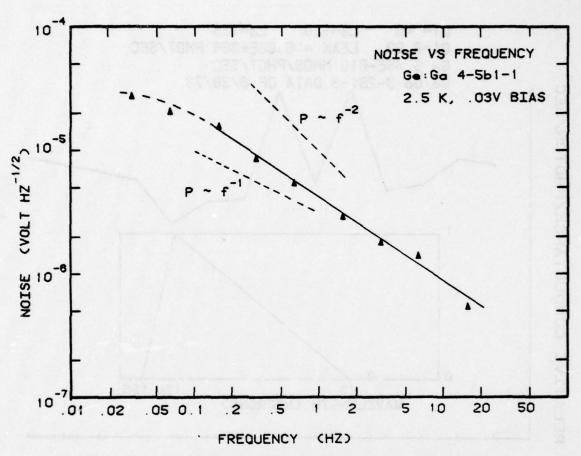


Fig. 15 — Noise vs frequency for sample 4-5bl-1. Data below about 0.1 Hz are uncertain due to interference from cosmic background radiation.

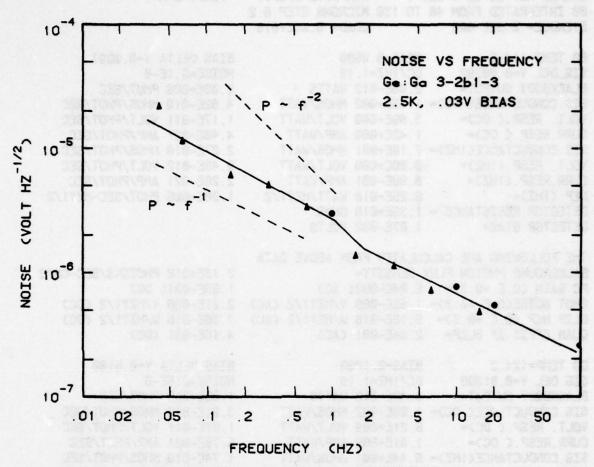


Fig. 16 — Noise vs frequency for sample 3-2bl-3

BB INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE = 2.35E-008 LOAD= 5.80E+818 88 TEMP-114.5 BIAS-0.9500 BIAS DELTA V-0.0097 SIG DEL V-0.00792 DC/1HZ=1.19 NOISE=6.1E-6 BLACKBODY OUTPUT= 2.86E-012 WATTS 9.03E+006 PHOT/SEC SIG. CONDUCTANCE(DC)= 1.46E+882 MHOS/WATT 4.62E-019 NHOS/PHOT/SEC VOLT. RESP. (DC)= 3.69E+009 VOLT/WATT 1.17E-011 VOLT/PHOT/SEC CURR.RESP. (DC)-1.42E+888 AMP/WATT 4.48E-021 AMP/PHOT/SEC SIG. CONDUCTANCE(1HZ)= 7.18E+801 MHOS/WATT 2.27E-019 NHOS/PHOT/SEC VOLT. RESP. (1HZ)= 3.00E+009 VOLT/WATT 9.48E-012 VOLT/PHOT/SEC CURR.RESP. (1HZ)= 6.96E-001 AMP/VATT 2.20E-021 AMP/PHOT/SEC 1.98E+005 PHOT/SEC-HZ11/2 NEP (IHZ)= 6.25E-016 WATT/HZ11/2 DETECTOR RESISTANCE = 1.35E+010 OHMS DETECTOR BIAS-1.07E-002 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 2.13E+010 PHOTONS/SEC-CMT2 PC GAIN (0.E.=0.3)= 5.04E-002(AC) 1.03E-001(DC) SHOT NOISE(Q.E.=0.3)= 1.55E-006 V/HZ11/2 (AC) 2.21E-006 V/HZ11/2 (DC) BLIP NEP (0.E.=0.3)- 5.16E-016 W/HZT1/2 (AC) 7.36E-016 W/HZT1/2 (DC) QUAN.EFFIC.IF BLIP-2.84E-881 (AC) 4.15E-001 (DC) BB TEMP-124.2 BIAS-0. 1000 BIAS DELTA V-0.0180 SIG DEL V-0.81396 DC/1HZ=1.19 NOISE=9.5E-6 BLACKBODY OUTPUT= 3.48E-012 WATTS 1.09E+009 PHOT/SEC SIG.CONDUCTANCE(DC)= 1.90E+802 MHOS/WATT 3.21E-819 NHOS/PHOT/SEC VOLT. RESP. (DC)-5.21E+889 VOLT/WATT 1.67E-011 VOLT/PHOT/SEC CURR.RESP. (DC)-1.61E+000 AMP/WATT 5.78E-021 AMP/PHOT/SEC SIG. CONDUCTANCE (!HZ) = 5.44E+881 MHOS/WATT 1.74E-019 NHOS/PHOT/SEC VOLT. RESP. (1HZ)= 4.25E+889 VOLT/WATT 1.36E-011 VOLT/PHOT/SEC 9.79E-901 AMP/WATT CURR.RESP. (1HZ)-3.13E-021 AMP/PHOT/SEC NEP (1HZ)-8.93E-016 WATT/HZ11/2 2.79E+005 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 1.23E+818 OHMS DETECTOR BIAS-1.98E-002 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 3.37E+010 PHOTONS/SEC-CMT2 PC GAIN (Q.E.=0.3)= 7.17E-002(AC) 1.32E-001(DC)

RUN DATE 5/5/77

TEMP.=3 K

2.29E-001 (DC)

SAMPLE NO. GE: GA 4-381-1

SHOT NOISE(Q.E.=0.3)= 2.44E-006 V/HZT1/2 (AC) 3.32E-006 V/HZT1/2 (DC) BLIP NEP (Q.E.=0.3)= 5.74E-016 W/HZT1/2 (AC) 7.80E-016 W/HZT1/2 (DC)

QUAN.EFFIC.IF BLIP- 1.24E-001 (AC)

TEMP.=3 K SAMPLE NO. GE: GA 4-381-1 RUN DATE 5/5/77
BB INTEGRATED FROM 48 TO 130 MICRONS STEP 8.2 ETENDUE= 2.35E-008 LOAD= 5.00E+010

2.68E-882 VOLTS

BB TEMP=114.8 BIAS=0.1500 BIAS DELTA V=0.0244
SIG DEL V=0.01700 DC/1HZ=1.19 NOISE=1.42E-5
BLACKBODY OUTPUT= 2.88E-012 WATTS 9.09E+008 PHOT/SEC SIG. CONDUCTANCE(DC)= 8.94E+881 NHOS/WATT 2.83E-819 NHOS/PHOT/SEC VOLT. RESP. (DC)= 7.42E+989 VOLT/WATT 2.3SE-811 VOLT/PHOT/SEC CURR.RESP. (DC)= 2.18E+898 AMP/WATT 6.98E-821 AMP/PHOT/SEC SIG. CONDUCTANCE (1HZ) = 5.49E+881 NHOS/WATT 1.74E-819 NHOS/PHOT/SEC VOLT. RESP. (1HZ)= 6.10E+009 VOLT/WATT 1.93E-011 VOLT/PHOT/SEC CURR.RESP. (1HZ)= 1.34E+888 AMP/WATT 4.24E-821 AMP/PHOT/SEC NEP (1HZ)= 1.08E-015 WATT/HZT1/2 3.41E+005 PHOT/SEC-HZT1/2 DETECTOR RESISTANCE = 1.89E+010 OHMS

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= PC GAIN (Q.E.=8.3)= 9.71E-882(AC) SHOT NOISE(Q.E.=0.3)= 3.18E-006 V/HZT1/2 (AC) 4.06E-006 V/HZT1/2 (DC)

BLIP NEP (Q.E.=0.3)= 5.22E-016 W/HZT1/2 (AC) 6.68E-016 W/HZT1/2 (DC)

QUAN.EFFIC.IF BLIP- 7.83E-802 (AC) 1.14E-801 (DC)

BB TEMP-101.5 BIAS-0.2000 CURR.RESP. (DC)- 2.97E+888 AMP/WATT
SIG.CONDUCTANCE(1HZ)- 6.41E+881 MHOS/WATT VOLT. RESP. (1HZ)-CURR.RESP. (1HZ)= NEP (1HZ)-

DETECTOR BIAS-

DETECTOR RESISTANCE = 1.81E+818 OHMS DETECTOR BIAS-3.36E-002 VOLTS

9.34E+009 VOLT/WATT 1.96E+000 AMP/WATT 1.95E-015 WATT/HZ11/2

BB TEMP=101.5

BIAS=0.2000

BIAS DELTA V=0.8306

SIG DEL V=0.81830

DC/1HZ=1.19

BLACKBODY OUTPUT= 2.89E-812 WATTS

SIG.CONDUCTANCE(DC)= 9.79E+881 MHOS/WATT

VOLT. RESP.(DC)= 1.13E+818 VOLT/WATT

SIG.CONDUCTANCE(DC)= 1.13E+818 VOLT/WATT BIAS DELTA V-0.0306 9.21E-821 AMP/PHOT/SEC 1.99E-019 NHOS/PHOT/SEC 2.90E-011 VOLT/PHOT/SEC

6.96E-921 AMP/PHOT/SEC

3.38E+005 PHOT/SEC-HZ11/2

4.33E+010 PHOTONS/SEC-CNT2

1.58E-001(DC)

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= PC GAIN (Q.E.=0.3)= 1.39E-001(AC) SHOT NOISE(Q.E.=0.3)= 4,17E-886 V/HZT1/2 (AC) 5.13E-886 V/HZT1/2 (DC)

QUAN.EFFIC.IF BLIP- 5.42E-002 (AC)

4.38E+018 PHOTONS/SEC-CMT2 2.11E-001(DC) BLIP NEP (Q.E.=0.3)- 4.46E-016 W/HZT1/2 (AC) 5.49E-016 W/HZT1/2 (DC) 8.21E-902 (DC)

SAMPLE NO: 8E:84 4=381-1 RUN DATE 3/28/77 TEMP.=2 K BB INTEGRATED FROM 40 TO 130 HICRONS STEP 0.2 ETENDUE= 2.35E-006 LOAD= 1.00E+011 BIAS-0.0200 BIAS DELTA V-0.0179 BB TEMP-195.1 DC/1HZ=2.9 SIG DEL V-0.01719 NOISE=2E-6 2.30E-012 WATTS 7.36E+006 PHOT/SEC BLACKBODY OUTPUT= SIG.CONDUCTANCE(DC)= 9.46E+801 MHOS/WATT 2.95E-819 MHOS/PHOT/SEC VOLT. RESP. (DC)= 1.35E+011 VOLT/WATT 4.29E-010 VOLT/PHOT/SEC CURR.RESP.(DC)= 1.69E+888 AMP/WATT
SIG.CONDUCTANCE(1HZ)= 2.17E+888 MHOS/WATT 5.29E-821 AMP/PHOT/SEC 6.79E-821 NHOS/PHOT/SEC VOLT. RESP. (1HZ)= 4.17E+888 VOLT/WATT 1.38E-811 VOLT/PHOT/SEC CURR. RESP. (1HZ)= 3.89E-002 AMP/WATT 1.22E-822 AMP/PHOT/SEC 4.75E-016 WATT/HZ11/2 NEP (1HZ)-1.52E+005 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 5.97E+012 OHMS DETECTOR BIAS-1.97E-002 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA 7.56E+007 PHOTONS/SEC-CM12 BACKGROUND PHOTON FLUX DENSITY= PC GAIN (Q.E.=0.3)= 2.78E-903(AC) 1.21E-001(DC) SHOT NOISE(Q.E.=0.3)= 2.17E-007 V/HZT1/2 (AC) 1.43E-006 V/HZT1/2 (DC) BLIP NEP (Q.E.=0.3)= 5.20E-017 W/HZT1/2 (AC) 3.43E-016 W/HZT1/2 (DC) QUAN.EFFIC.IF BLIP-1.58E-001 (DC) 3.58E-003 (AC) 88 TEMP-184.5 BIAS DELTA V-8.8445 BIAS-0.0500 SIG DEL V-0.04250 DC/1HZ=2.9 NOTSE=2.8E-6 2.26E-012 WATTS 7.25E+898 PHOT/SEC BLACKBODY OUTPUT= SIG. CONDUCTANCE(DC)= 9.68E+881 HHOS/WATT 3.88E-819 MHOS/PHOT/SEC VOLT. RESP. (DC)-3.13E+011 VOLT/WATT 9.76E-010 VOLT/PHOT/SEC CURR.RESP. (DC)= 4.27E+999 AMP/WATT 1.39E-020 AMP/PHOT/SEC SIG. CONDUCTANCE(1HZ)= 2.22E+888 NHOS/WATT 6.92E-021 NHOS/PHOT/SEC 3.27E-011 VOLT/PHOT/SEC VOLT. RESP. (1HZ)= 1.85E+010 VOLT/WATT 9.88E-002 AMP/WATT 3. DEE-022 AMP/PHOT/SEC CURR.RESP.(1HZ)= 8.48E+004 PHOT/SEC-HZ11/2 NEP (1HZ)-2.64E-816 WATT/HZT1/2 DETECTOR RESISTANCE = 4.45E+012 OHMS DETECTOR BIAS-4.89E-002 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA

SHOT NOISE(Q.E.=0.3)= 6.27E-887 V/HZ11/2 (AC) 4.12E-886 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)= 5.97E-817 W/HZ11/2 (AC) 3.93E-816 W/HZ11/2 (DC)

BACKGROUND PHOTON FLUX DENSITY=

PC GAIN (Q.E.=0.3)= 7.05E-003(AC)

QUAN. EFFIC. IF BLIP- 1.54E-802 (AC)

1.99E+996 PHOTONS/SEC-CHT2

3.95E-901(DC)

6.65E-001 (DC)

SAMPLE NO. GE: GA 4-381-1 RUN DATE 3/28/77 TEMP.=2 K BB INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE= 2.35E-808 LOAD= 1.99E+011 BB TEMP- 76.8 BIAS-0.0200 SIG DEL V-0.01200 DC/1HZ-2.9 BIAS DELTA V-0.0180 NOISE=2E-6 NEP (1HZ)-2.84E-816 WATT/HZ11/2 9.69E+884 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 9.88E+812 OHMS DETECTOR BIAS- 1.98E-882 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKEROUND PHOTON FLUX DENSITY= 1.82E+008 PHOTONS/SEC-CMT2 PC GAIN (Q.E.=0.3)- 4.35E-003(AC) 3.35E-002(DC) SHOT NOISE(Q.E.=0.3)= 2.23E-807 V/HZT1/2 (AC) 6.18E-807 V/HZT1/2 (DC) BLIP NEP (Q.E.=0.3)= 3.17E-017 W/HZ11/2 (AC) 8.88E-017 W/HZ11/2 (DC) QUAN.EFFIC.IF BLIP- 3.74E-983 (AC) 2.88E-982 (DC) BIAS DELTA V-0.0458 BB TEMP- 78.5 BTAS-0.0500 STG DEL V-0.83458 DC/1HZ=2.9 NOTSE=2.8E-6
BLACKBODY OUTPUT= 9.10E-013 WATTS 3.11E+008 PHOT/SEC
STG.CONDUCTANCE(DC)= 3.33E+001 PHOS/WATT 9.76E-029 PHOS/PHOT/SEC
VOLT. RESP. (DC)= 1.72E+011 VOLT/WATT 5.04E-018 VOLT/PHOT/SEC CURR.RESP. C DC)= 1.S3E+999 AMP/WATT
SIG.CONDUCTANCE(1HZ)= 3.83E+999 MHOS/WATT
VOLT. RESP. C1HZ)= 1.95E+910 VOLT/WATT 4.47E-021 AMP/PHOT/SEC 1.12E-028 HHOS/PHOT/SEC 1.44E-016 WATT/HZT1/2 4.93E+004 PHOT/SEC -1.53E+013 (HMS CURR.RESP.(1HZ)-NEP (1HZ)= 4.93E+804 PHOT/SEC-HZ11/2

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY-PC GAIN (0.E.=0.3)- 1.18E-082(AC) SHOT NOISE(0.E.=0.3)= 4.50E-007 V/HZT1/2 (AC) 1.33E-006 V/HZT1/2 (DC) BLIP NEP (Q.E.=0.3)- 2.31E-017 W/HZT1/2 (AC) 6.83E-017 W/HZT1/2 (DC) QUAN.EFFIC.IF BLIP- 7.72E-003 (AC) 6.72E-002 (DC)

5.83E-982 VOLTS

DETECTOR RESISTANCE =-1.53E+013 OHMS

DETECTOR BIAS-

8.95E+007 PHOTONS/SEC-CHT2 1.02E-001(DC)

TEMP. =3 K BB INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-009 LOAD= 5.88E+818 BB TEMP- 59.5 BIAS-0.0050 BIAS DELTA V-0.0030 SIG DEL V-0.00120 DC/1HZ=2 NOISE=2E-6 BLACKBODY OUTPUT= 1.10E-013 WATTS 4.82E+887 PHOT/SEC SIG. CONDUCTANCE(DC)= 1.84E+882 NHOS/WATT 5.03E-019 MHOS/PHOT/SEC VOLT. RESP. (DC)-1.63E+010 VOLT/WATT 4.45E-011 VOLT/PHOT/SEC CURR.RESP. (DC)= 5.53E-001 AMP/WATT 1.51E-021 AMP/PHOT/SEC SIG. CONDUCTANCE(1HZ)= 6.91E+001 MHOS/WATT 1.89E-019 NHOS/PHOT/SEC 1.89E-011 VOLT/PHOT/SEC 6.92E+009 VOLT/WATT VOLT. RESP. (1HZ)= CURR.RESP.(1HZ)= 2.87E-881 AMP/WATT 5.66E-822 AMP/PHOT/SEC 2.56E-016 WATT/HZ11/2 9.76E+884 PHOT/SEC-HZ11/2 NEP (1HZ)-DETECTOR RESISTANCE = 9.66E+010 OHMS DETECTOR BIAS-3.30E-003 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA 2.74E+009 PHOTONS/SEC-CH12 BACKGROUND PHOTON FLUX DENSITY= 3.45E-002(DC) 1.30E-002(AC) PC GAIN (Q.E.=0.3)-SHOT NOISE(Q.E.=0.3)= 5.04E-007 V/HZ11/2 (AC) 8.25E-007 V/HZT1/2 (DC) BLIP NEP (0.E.=0.3)= 7.28E-017 W/HZ11/2 (AC) 1.19E-016 W/HZ11/2 (DC) QUAN. EFFIC. IF BLIP-2.24E-002 (AC) 5.99E-002 (DC) BIAS DELTA V-0.0058 88 TEMP- 59.2 BIAS-0.9100 SIG DEL V-0.88225 NOISE=2.2E-6 DC/1HZ=2 1.00E-013 WATTS BLACKBODY OUTPUT= 3.95E+007 PHOT/SEC SIG. CONDUCTANCE(DC)= 1.65E+882 NHOS/WATT 5.83E-819 NHOS/PHOT/SEC VOLT. RESP. (DC)= 3.85E+010 VOLT/WATT 8.31E-011 VOLT/PHOT/SEC CURR.RESP. (DC)-1.97E+999 AMP/WATT 2.92E-021 AMP/PHOT/SEC SIG. CONDUCTANCE(1HZ)= 7.82E+881 MHOS/WATT 1.91E-019 NHOS/PHOT/SEC 1.31E+010 VOLT/WATT 3.57E-011 VOLT/PHOT/SEC VOLT. RESP. (1HZ)-4.87E-881 AMP/WATT CURR.RESP. (1HZ)-1.11E-021 AMP/PHOT/SEC 1.54E-016 WATT/HZT1/2 NEP (1HZ)= 5.67E+004 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 8.79E+010 OHMS DETECTOR BIAS-6.37E-993 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA 3.81E+889 PHOTONS/SEC-CMT2 BACKGROUND PHOTON FLUX DENSITY= 6.68E-982(DC) 1.62E-986 V/HZT1/2 (DC) 2.54E-002(AC) PC GAIN (Q.E.=8.3)-

RUN DATE 6/9/78

SAMPLE NO. GE:GA 3-2B1-3

BLIP NEP (0.E.=0.3)= 7.59E-017 W/HZT1/2 (AC) 1.29E-016 W/HZT1/2 (DC)

1.91E-001 (DC)

SHOT NOISE(Q.E.=0.3)= 9.95E-007 V/HZ11/2 (AC)

CLIAN EFFIC. IF BLIP- 7.26E-982 (AC)

TEMP.=3 K SAMPLE NO. GE: GA 3-281-3 RUN DATE 6/9/78 BB TEMP- 59.2 BIAS-0.0200 BIAS DELTA V-0.0110 SIG DEL V-0.90382 BLACKBODY OUTPUT= DC/1HZ=2 NOISE=3.6E-6 1.96E-013 WATTS 3.95E+007 PHOT/SEC SIG. CONDUCTANCE(DC)= 1.64E+882 MHOS/WATT 4.46E-819 MHOS/PHOT/SEC VOLT. RESP. (DC)- 4.94E+010 VOLT/WATT 1.34E-010 VOLT/PHOT/SEC 1.89E+000 AMP/WATT CURR.RESP. (DC)-4.90E-021 AMP/PHOT/SEC SIG. CONDUCTANCE(1HZ)= 6.46E+881 HHOS/WATT 1.76E-819 NHOS/PHOT/SEC 2.18E+010 VOLT/WATT 5.94E-011 VOLT/PHOT/SEC 7.11E-001 AMP/WATT 1.94E-021 AMP/PHOT/SEC VOLT. RESP. (1HZ)-CURR.RESP.(1HZ)= 1.53E-016 WATT/HZT1/2 5.60E+004 PHOT/SEC-HZ11/2 NEP (1HZ)= DETECTOR RESISTANCE = 7.64E+010 OHMS DETECTOR BIAS- 1.21E-902 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA 3.92E+889 PHOTONS/SEC-CMT2 BACKGROUND PHOTON FLUX DENSITY= PC GAIN (Q.E.=0.3)= 4.43E-002(AC) 1.12E-801(DC) SHOT NOISE(Q.E.=0.3)= 1.84E-006 V/HZ11/2 (AC) 2.93E-006 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)= 8.48E-017 W/HZ11/2 (AC) 1.3SE-016 W/HZ11/2 (DC) QUAN.EFFIC.IF BLIP- 9.22E-002 (AC) 2.33E-001 (DC) 88 TEMP- 69.5 BIAS-0.0300 BIAS DELTA V-0.0155 DC/1HZ=2 NOISE=4.6E-6 SIG DEL V-0.90590 1.17E-013 WATTS 4.26E+907 PHOT/SEC BLACKBODY OUTPUT= SIG.CONDUCTANCE(DC)= 1.85E+882 MHOS/WATT
VOLT. RESP.(DC)= 7.85E+818 VOLT/WATT
CURR.RESP.(DC)= 2.87E+888 AMP/WATT 5.88E-819 NHOS/PHOT/SEC 1.94E-010 VOLT/PHOT/SEC 7.88E-021 AMP/PHOT/SEC SIG. CONDUCTANCE (1HZ)= 7.89E+881 NHOS/WATT 1.94E-819 NHOS/PHOT/SEC 3.11E+010 VOLT/WATT 1.10E+000 AMP/WATT VOLT. RESP. (1HZ)= 8.53E-011 VOLT/PHOT/SEC 3.01E-021 AMP/PHOT/SEC CURR.RESP.(1HZ)= NEP (1HZ)-1.34E-016 WATT/HZ11/2 4.89E+004 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 6.57E+819 OHMS DETECTOR BIAS- 1.79E-902 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 3.99E+989 PHOTONS/SEC-CMT PC GAIN (D.E.=8.3)= 6.99E-982(AC) 1.89E-981(DC) 3.99E+009 PHOTONS/SEC-CMT2 SHOT NOISE(Q.E.=0.3)= 2.76E-006 V/HZT1/2 (AC) 4.47E-006 V/HZT1/2 (DC)

BLIP NEP (0.E.=0.3)- 8.68E-017 W/HZT1/2 (AC) 1.44E-016 W/HZT1/2 (DC)

3.44E-991 (DC)

QUAN.EFFIC.IF BLIP- 1.31E-001 (AC)

88 INTEGRATED FROM 48 TO 138 HICRONS STEP 8.2 ETENDUE= 6.84E-000 LOAD= 5.80E+018 BIAS-0.0490 BIAS DELTA V-9.9189 BB TEMP- 59.2 DC/1HZ=2 SIG DEL V-0. 90669 NOTSE=6E-6 3.95E+907 PHOT/SEC BLACKBODY OUTPUT= 1.98E-813 WATTS SIG. CONDUCTANCE(DC)= 1.92E+802 NHOS/WATT 5.25E-819 NHOS/PHOT/SEC VOLT. RESP. (DC)- 8.25E+818 VOLT/WATT 2.24E-010 VOLT/PHOT/SEC 3.63E+000 AMP/WATT 9.89E-021 AMP/PHOT/SEC CURR.RESP. (DC)-STG. CONDUCTANCE (1HZ)- 7.57E+881 HHOS/WATT 2.86E-819 NHOS/PHOT/SEC VOLT. RESP. (1HZ)- 3.71E+818 VOLT/WATT 1.81E-818 VOLT/PHOT/SEC CURR.RESP.(1HZ)= 1.43E+888 AMP/WATT 3.90E-021 AMP/PHOT/SEC 1.47E-016 WATT/HZT1/2 5.48E+884 PHOT/SEC-HZ11/2 NEP (1HZ)= DETECTOR RESISTANCE = 5.49E+019 OHMS DETECTOR BIAS-2.86E-882 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA 4.72E+009 PHOTONS/SEC-CHT2 BACKGROUND PHOTON FLUX DENSITY= 2.26E-001(DC) PC GAIN (Q.E.=0.3)= 8.92E-802(AC) SHOT NOTSE(Q.E.=0.3)= 3.58E-886 V/HZ11/2 (AC) 5.58E-886 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)= 9.45E-017 W/HZT1/2 (AC) 1.50E-016 W/HZT1/2 (DC) QUAN. EFFIC. IF BLIP- 1.24E-001 (AC) 3.15E-001 (DC) BIAS-0.0500 BIAS DELTA V-0.0230 88 TEMP- 59.9 SIG DEL V-0.80780 DC/1HZ-2 NOTSE=6E-6 1.96E-013 WATTS 3.90E+007 PHOT/SEC BLACKBODY OUTPUT= SIE CONDUCTANCEC DC>= 1.63E+002 HHOS/WATT 4.49E-019 NHOS/PHOT/SEC VOLT. RESP. (DC)= 8.56E+818 VOLT/WATT 2.33E-010 VOLT/PHOT/SEC CURR.RESP.(DC)= 3.75E+888 AMP/WATT
SIG.CONDUCTANCE(1HZ)= 6.86E+881 MHOS/WATT 1.82E-829 AMP/PHOT/SEC

3.92E+010 VOLT/WATT

1.41E-016 WATT/HZT1/2

1.54E+000 AMP/WATT

2.53E-002 VOLTS

SAMPLE NO. GE:GA 3-281-3 RUN DATE 6/9/78 TEMP.=3 K

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY-PC GAIN (Q.E.=0.3)- 9.58E-002(AC) SHOT NOISE(Q.E.=0.3)= 4.00E-006 V/HZ11/2 (AC) 6.25E-006 V/HZ11/2 (DC) BLIP NEP (0.E.=0.3)- 1.82E-016 W/HZ11/2 (AC) 1.59E-016 W/HZ11/2 (DC) QUAN.EFFIC.IF BLIP- 1.58E-001 (AC)

DETECTOR RESISTANCE = 5.11E+818 OHMS

VOLT. RESP. (1HZ)-CURR.RESP. (1HZ)-

NEP (1HZ)-

DETECTOR BIAS-

5.88E+889 PHOTONS/SEC-CMT2 2.35E-001(DC) 3.86E-001 (DC)

1.82E-818 NHOS/PHOT/SEC 1.87E-018 VOLT/PHOT/SEC

4.18E-021 AMP/PHOT/SEC 5.18E+004 PHOT/SEC-HZ11/2

The state of the s

TEMP.=3 K SAMPLE NO. GE: GA 3-281-3 RUN DATE 6/9/78 88 INTEGRATED FROM 40 TO 130 HICRONS STEP 0.2 LOAD- 5.00E+010 ETENDUE= 6.84E-009 BIAS-0.0500 BIAS DELTA V-0.8230 88 TEMP- 59.8 SIG DEL V-0.00740 DC/1HZ-2 NOISE=6E-6 3.99E+007 PHOT/SEC BLACKBODY OUTPUT= 1.96E-013 WATTS SIG.CONDUCTANCE(DC)= 1.77E+802 NHOS/WATT 4.81E-019 NHOS/PHOT/SEC VOLT. RESP. (DC)- 9.14E+818 VOLT/WATT 2.49E-010 VOLT/PHOT/SEC CURR.RESP. (DC)= 4.96E+999 AMP/WATT 1.11E-929 AMP/PHOT/SEC SIG.CONDUCTANCE(1HZ)= 7.14E+991 MHOS/WATT 1.94E-919 MHOS/PHOT/SEC VOLT. RESP. (1HZ)= 4.17E+010 VOLT/WATT 1.13E-010 VOLT/PHOT/SEC CURR.RESP. (1HZ)= 1.64E+000 AMP/WATT 4.47E-021 AMP/PHOT/SEC 1.32E-016 WATT/HZ11/2 4.83E+004 PHOT/SEC-HZ11/2 NEP (1HZ)= DETECTOR RESISTANCE = 5.11E+010 OHMS DETECTOR BIAS-2.53E-002 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 5.43E+009 PHOTONS/SEC-CHT2 PC GAIN (Q.E.=9.3)= 1.82E-981(AC) 2.53E-801(DC) SHOT NOISE(Q.E.=0.3)= 4.14E-006 V/HZT1/2 (AC) 6.51E-006 V/HZT1/2 (DC) BLIP NEP (Q.E.=0.3)= 9.93E-017 W/HZ11/2 (AC) 1.56E-016 W/HZ11/2 (DC) QUAN.EFFIC.IF BLIP- 1.71E-901 (AC) 4.23E-001 (DC) BIAS DELTA V-0.0244 BB TEMP- 59.9 BIAS-0.9699 SIG DEL V-8.99829 DC/1HZ=2 NOISE=7.5E-6 1.86E-813 WATTS 3.98E+887 PHOT/SEC BLACKBODY OUTPUT= SIG.CONDUCTANCE(DC)= 2.13E+002 MHOS/WATT 5.80E-019 MHOS/PHOT/SEC VOLT. RESP.(DC)= 9.90E+010 VOLT/WATT 2.72E-010 VOLT/PHOT/SEC CURR.RESP.(DC)= 5.20E+000 AMP/WATT 1.42E-020 AMP/PHOT/SEC SIG.CONDUCTANCE(1HZ)= 8.51E+001 MHOS/WATT 2.32E-019 MHOS/PHOT/SEC VOLT/PHOT/SEC V VOLT. RESP. (1HZ)-4.58E+010 VOLT/WATT 1.25E-010 VOLT/PHOT/SEC CURR.RESP. (1HZ)-2.06E+000 AMP/WATT 5.65E-021 AMP/PHOT/SEC NEP (1HZ)-1.47E-016 WATT/HZ11/2 5.41E+004 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 4.84E+818 OHMS DETECTOR BIAS- 2.68E-082 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY=
PC GAIN (D.E.=0.3)= 1.29E-001(AC) 5.69E+009 PHOTONS/SEC-CMT2 3.24E-001(DC) SHOT NOISE(Q.E.=8.3)= 4.77E-886 V/HZ11/2 (AC) 7.54E-886 V/HZ11/2 (DC)

BLIP NEP (Q.E.=0.3)- 1.04E-016 W/HZ11/2 (AC) 1.65E-016 W/HZ11/2 (DC)
QUAN.EFFIC.IF BLIP- 1.50E-001 (AC) 3.75E-001 (DC)

TEMP.=3 K SAMPLE NO. GE: GA 3-281-3 RUN DATE 6/9/78 88 INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-009 LOAD= 5.80E+010

BB TEMP- 59.8 BIAS-0.0700 BIAS DELTA V-0.0248 SIG DEL V-0.00850 DC/1HZ=2 NOISE=8E-6 BLACKBODY OUTPUT= 1.06E-013 WATTS 3.90E+007 PHOT/SEC SIG. CONDUCTANCE(DC)= 2.52E+002 MHOS/WATT 6.86E-019 NHOS/PHOT/SEC 1.01E+011 VOLT/WATT VOLT. RESP. (DC)-2.76E-010 VOLT/PHOT/SEC CURR.RESP. (DC)= 6.25E+000 AMP/WATT 1.78E-029 AMP/PHOT/SEC SIG. CONDUCTANCE (1HZ)= 1.88E+882 NHOS/WATT 2.72E-819 NHOS/PHOT/SEC 4.71E+818 VOLT/WATT 1.28E-010 VOLT/PHOT/SEC VOLT. RESP. (1HZ)-2.48E+999 AMP/WATT CURR.RESP. (1HZ)= 6.75E-021 AMP/PHOT/SEC NEP (1HZ)-1.51E-016 WATT/HZT1/2 5.54E+004 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 3.19E+010 OHMS 2.73E-002 VOLTS DETECTOR BIAS-

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= PC GAIN (Q.E.=0.3)= 1.54E-001(AC) SHOT NOISE(Q.E.=0.3)= 5.15E-006 V/HZ11/2 (AC) BLIP NEP (0.E.=0.3)= 1.89E-016 W/HZT1/2 (AC) 1.74E-016 W/HZT1/2 (DC) CLIAN EFFIC IF BLIP- 1.58E-001 (AC)

6.10E+009 PHOTONS/SEC-CHT2 3.90E-001(DC) 8.18E-006 V/HZT1/2 (DC) 3.98E-001 (DC)

BB TEMP- 58.9 BIAS-0.0800 SIG DEL V-0.01100 DC/1HZ=2 BLACKBODY OUTPUT= 1.06E-013 WATTS SIG. CONDUCTANCE(DC)= 2.96E+082 MHOS/WATT VOLT. RESP. (DC)-1.35E+011 VOLT/WATT CURR.RESP. (DC)= 8.52E+000 AMP/WATT SIG. CONDUCTANCE(1HZ)= 1.13E+802 NHOS/WATT VOLT. RESP. (1HZ)= 6.19E+010 VOLT/WATT CURR.RESP. (1HZ)-3.26E+000 AMP/WATT NEP (1HZ)-1.28E-016 WATT/HZT1/2 DETECTOR RESISTANCE = 3.27E+018 OHMS DETECTOR BIAS-3.16E-002 VOLTS

BIAS DELTA V-0. 2288 NOISE=8.5E-6 3.88E+007 PHOT/SEC 8.85E-819 MHOS/PHOT/SEC 3.67E-010 VOLT/PHOT/SEC 2.32E-829 AMP/PHOT/SEC 3.97E-019 MHOS/PHOT/SEC 1.68E-010 VOLT/PHOT/SEC 8.85E-821 AMP/PHOT/SEC 4.42E+004 PHOT/SEC-HZT1/2

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY-PC GAIN (Q.E.=0.3)= 2.83E-801(AC) SHOT NOISE(Q.E.=0.3)= 6.38E-986 V/HZT1/2 (AC) 1.83E-985 V/HZT1/2 (DC) BLIP NEP (Q.E.=0.3)- 1.83E-016 W/HZT1/2 (AC) 1.67E-016 W/HZT1/2 (DC) QUAN. EFFIC. IF BLIP- 2.29E-901 (AC)

5.06E+009 PHOTONS/SEC-CMT2 5.31E-001(DC) 5.77E-981 (DC)

BB INTEGRATED FROM 48 TO 138 MICRONS STEP 8.2 ETENDUE= 6.84E-000 LOAD= 5.00E+010 BB TEMP- 58.9 BIAS-0.8900 BIAS DELTA V-0.0295 SIG DEL V-0.00065 DC/1HZ-2 NOISE=9E-6 BLACKBODY OUTPUT= 1.96E-013 WATTS 3.88E+007 PHOT/SEC SIG. CONDUCTANCE(DC)= 2.52E+882 NHOS/WATT 6.85E-819 NHOS/PHOT/SEC VOLT. RESP. (DC)= 1.13E+011 VOLT/WATT 3.06E-010 VOLT/PHOT/SEC CURR.RESP. (DC)= 7.43E+000 AMP/WATT 2.02E-020 AMP/PHOT/SEC SIG.CONDUCTANCE(1HZ)= 1.02E+002 MHOS/VATT 2.76E-019 MHOS/PHOT/SEC VOLT. RESP.(1HZ)= 5.28E+010 VOLT/WATT 1.44E-010 VOLT/PHOT/SEC CURR.RESP.(1HZ)= 3.00E+000 ANP/WATT 8.15E-021 AMP/PHOT/SEC NEP (1HZ)= 1.52E-016 WATT/HZT1/2 5.58E+004 PHOT/SEC-HZT1/2 DETECTOR RESISTANCE = 2.81E+010 OHMS DETECTOR BIAS- 3.24E-902 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 6.92E+009 PHOTONS/SEC-CHT2 PC GAIN (Q.E.=0.3)= 1.87E-001(AC) 4.62E-001(DC) SHOT NOISE(Q.E.=0.3)= 6.00E-006 V/HZ11/2 (AC) 9.57E-006 V/HZ11/2 (DC) BLIP NEP (0.E.=0.3)= 1.15E-016 W/HZT1/2 (AC) 1.81E-016 W/HZT1/2 (DC) QUAN.EFFIC.IF BLIP- 1.73E-801 (AC) 4.28E-801 (DC) BB TEMP- 58.8 BIAS-0.1000 BIAS DELTA V=0.0316 SIG DEL V-0.01010 DC/1HZ=2 NOISE=1E-5 BLACKBODY OUTPUT= 1.05E-013 WATTS 3.86E+007 PHOT/SEC SIG. CONDUCTANCE(DC)= 2.58E+882 MHOS/WATT 7.01E-019 MHOS/PHOT/SEC VOLT. RESP. (DC)= 1.19E+011 VOLT/WATT 3.24E-010 VOLT/PHOT/SEC CURR.RESP. (DC)= 8.15E+000 AMP/WATT 2.22E-020 AMP/PHOT/SEC SIG. CONDUCTANCE(1HZ)= 1.94E+992 MHOS/WATT 2.84E-919 MHOS/PHOT/SEC VOLT. RESP. (1HZ)= 5.68E+810 VOLT/WATT 1.52E-810 VOLT/PHOT/SEC CURR.RESP.(1HZ)= 3.30E+000 AMP/WATT 8.97E-021 AMP/PHOT/SEC NEP (1HZ)= 1.59E-016 WATT/HZT1/2 5.84E+004 PHOT/SEC-HZT1/2 DETECTOR RESISTANCE = 2.66E+010 OHMS DETECTOR BIAS- 3.47E-902 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 7.15E+889 PHOTONS/SEC-CHT2
PC GAIN (0.E.=0.3)= 2.85E-881(AC) 5.87E-881(DC) SHOT NOISE(Q.E.=0.3)= 6.55E-006 V/HZT1/2 (AC) 1.03E-005 V/HZT1/2 (DC)

TEMP.=3 K

SAMPLE NO. GE: GA 3-281-3 RUN DATE 6/9/78

BLIP NEP (Q.E.=0.3)- 1.17E-016 W/HZT1/2 (AC) 1.84E-016 W/HZT1/2 (DC)
QUAN.EFFIC.IF BLIP- 1.62E-001 (AC) 4.01E-001 (DC)

BB INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-009 LOAD= 7.00E+010 BIAS-0.0050 BB TEMP- 59.0 BIAS DELTA V=0.9041 SIG DEL V-0.00202 DC/1HZ-2.2 NOISE=2.5E-6 BLACKBODY OUTPUT= 1.86E-913 WAT: 3.98E+987 PHOT/SEC SIG.CONDUCTANCE(DC)= 1.46E+882 HHOS/VATT 3.97E-819 HHOS/PHOT/SEC VOLT. RESP. (DC)= 3.76E+010 VOLT/WATT 1.02E-010 VOLT/PHOT/SEC CURR.RESP. (DC)= 5.97E-001 AMP/WATT 1.62E-021 AMP/PHOT/SEC SIG.CONDUCTANCE(1HZ)= 4.33E+801 MHOS/VATT 1.18E-819 MHOS/PHOT/SEC VOLT. RESP. (1HZ)= 1.19E+010 VOLT/WATT 3.24E-011 VOLT/PHOT/SEC CURR.RESP.(1HZ)= 1.77E-801 AMP/WATT 4.82E-822 AMP/PHOT/SEC 7.50E+004 PHOT/SEC-HZ11/2 NEP (1HZ)= 2.04E-016 WATT/HZ11/2 DETECTOR RESISTANCE = 6.22E+011 OHMS DETECTOR BIAS- 4.49E-003 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 5.39E+008 PHOTONS/SEC-CMT2 PC GAIN (Q.E.=0.3)= 1.10E-002(AC) 3.72E-002(DC) SHOT NOISE(Q.E.=0.3)= 4.89E-807 V/HZ11/2 (AC) 7.51E-807 V/HZ11/2 (DC) BLIP NEP (0.E.=0.3)= 3.44E-017 W/HZ11/2 (AC) 6.31E-017 W/HZ11/2 (DC) QUAN. EFFIC. IF BLIP= 8.50E-003 (AC) 2.87E-002 (DC) BIAS-0.0100 BIAS DELTA V=0.9984 BB TEMP- 58.9 SIG DEL V=0.88419 DC/1HZ=2.2 NOISE=2.5E-6
BLACKBODY OUTPUT= 1.86E-013 WATTS 3.88E+907 PHOT/SEC SIG.CONDUCTANCE(DC)= 1.47E+892 MHOS/WATT 4.89E-819 MHOS/PHOT/SEC VOLT. RESP. (DC)= 8.86E+818 VOLT/WATT 2.28E-818 VOLT/PHOT/SEC CURR.RESP. (DC)= 1.23E+888 AMP/WATT 3.3SE-821 AMP/PHOT/SEC SIG.CONDUCTANCE(1HZ)= 4.32E+801 MHOS/VATT 1.18E-019 MHOS/PHOT/SEC VOLT. RESP. (1HZ)= 2.51E+010 VOLT/WATT 6.82E-011 VOLT/PHOT/SEC CURR.RESP.(1HZ)= 3.62E-901 AMP/WATT 9.85E-922 AMP/PHOT/SEC 9.74E-017 WATT/HZT1/2 3.58E+004 PHOT/SEC-HZT1/2 NEP (1HZ)= DETECTOR RESISTANCE = 8.15E+011 OHMS DETECTOR BIAS-9.21E-003 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 4.89E+888 PHOTONS/SEC-CMT2 PC GAIN (D.E.=0.3)= 2.28E-002(AC) 7.87E-202(DC) SHOT NOISE(Q.E.=0.3)= 7.49E-807 V/HZ11/2 (AC) 1.38E-806 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)- 2.99E-017 W/HZT1/2 (AC) 5.51E-017 W/HZT1/2 (DC)

SAMPLE NO. GE:GA 3-281-3 RUN DATE 6/9/78 TEMP.=2.5 K

QUAN.EFFIC.IF BLIP= 2.82E-002 (AC) 9.59E-002 (DC)

TEMP.=2.5 K SAMPLE NO. GE:GA 3-2B1-3 RUN DATE 6/9/78 BB INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-009 LOAD= 7.88E+818

BB TEMP- 58.8 BIAS-0.0100 BIAS DELTA V-0.0081 SIG DEL V-0.00395 DC/1HZ=2.2 NOISE=2.5E-6 BLACKBODY OUTPUT= 1.86E-813 WATTS 3.86E+807 PHOT/SEC SIG. CONDUCTANCE(DC)= 1.46E+882 MHOS/WATT 3.96E-819 MHOS/PHOT/SEC VOLT. RESP. (DC)= 7.31E+818 VOLT/WATT 1.99E-818 VOLT/PHOT/SEC CURR.RESP. (DC)= 1.18E+888 AMP/WATT 3.21E-821 AMP/PHOT/SEC SIG.CONDUCTANCE(1HZ)= 4.36E+881 NHOS/WATT 1.18E-819 NHOS/PHOT/SEC VOLT. RESP. (1HZ)= 2.34E+010 VOLT/WATT 6.37E-011 VOLT/PHOT/SEC CURR. RESP. (1HZ)= 3.53E-001 AMP/WATT 9.60E-022 AMP/PHOT/SEC NEP (1HZ)= 1.83E-816 WATT/HZ11/2 3.81E+884 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 5.67E+011 OHMS DETECTOR BIAS-8.90E-003 VOLTS

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= PC GAIN (Q.E.=0.3)= 2.29E-902(AC) SHOT NOISE(0.E.=0.3)= 8.42E-807 V/HZT1/2 (AC) 1.54E-806 V/HZT1/2 (DC)

BLIP NEP (Q.E.=0.3)= 3.59E-017 W/HZT1/2 (AC) 6.57E-017 W/HZT1/2 (DC) QUAN. EFFIC. IF BLIP- 3.62E-002 (AC)

BB TEMP= 58.8 BIAS=0.0200 SIG DEL V-0.00025 DC/1HZ-2.2 NOISE-2.5E-6 BLACKBODY OUTPUT= 1.95E-813 WATTS 3.88E+997 PHOT/SEC SIG. CONDUCTANCE(DC)= 1.65E+882 HHOS/WATT 4.48E-819 HHOS/PHOT/SEC VOLT. RESP. (DC)= 1.58E+811 VOLT/WATT 4.38E-818 VOLT/PHOT/SEC CURR.RESP. (DC)= 2.64E+888 AMP/WATT 7.17E-821 AMP/PHOT/SEC SIG. CONDUCTANCE (1HZ)= 4.74E+881 MHOS/WATT 1.29E-818 MHOS/PHOT/SEC VOLT. RESP. (1HZ)= 4.95E+010 VOLT/WATT 1.35E-010 VOLT/PHOT/SEC 7.59E-001 AMP/WATT CURR.RESP.(1HZ)-NEP (1HZ)= DETECTOR RESISTANCE = 5.89E+811 OHMS DETECTOR BIAS- 1.76E-882 VOLTS

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY-PC GAIN (O.E.=0.3)- 4.72E-882(AC) 1.64E-881(DC) SHOT NOISE(Q.E.=0.3)= 1.81E-006 V/HZ11/2 (AC) 3.37E-006 V/HZ11/2 (DC)

QUAN. EFFIC. IF BLIP- 1.89E-001 (AC)

5.94E+008 PHOTONS/SEC-CHT2 7.34E-002(DC) 1.21E-001 (DC)

BIAS DELTA V=0.0160 2.06E-021 AMP/PHOT/SEC 4.87E-817 WATT/HZ11/2 1.79E+884 PHOT/SEC-HZ11/2

5.84E+998 PHOTONS/SEC-CHT2 BLIP NEP (Q.E.=0.3)- 3.66E-017 W/HZ11/2 (AC) 6.82E-017 W/HZ11/2 (DC) 5.88E-001 (DC)

BB INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-889 LOAD= 7.88E+818 BB TEMP- 58.8 BIAS-0.0300 SIG DEL V-0.01250 DC/1HZ-2.2 BIAS DELTA V=0.0234 NOISE=UNDEFINEDQ BLACKBODY OUTPUT= 1.85E-013 WATTS 3.86E+807 PHOT/SEC SIG. CONDUCTANCE(DC)= 1.82E+882 MHOS/WATT 4.95E-819 MHOS/PHOT/SEC VOLT. RESP. (DC)- 2.42E+011 VOLT/WATT 6.57E-010 VOLT/PHOT/SEC CURR.RESP. (DC)= 4.26E+888 AMP/WATT 1.16E-828 AMP/PHOT/SEC SIG. CONDUCTANCE (1HZ)= 5.10E+001 MHOS/WATT 1.39E-019 MHOS/PHOT/SEC VOLT. RESP. (1HZ)= 7.52E+818 VOLT/WATT 2.84E-818 VOLT/PHOT/SEC CURR.RESP. (1HZ)= 1.19E+000 AMP/WATT 3.24E-021 AMP/PHOT/SEC DETECTOR RESISTANCE = 4.20E+011 OHMS DETECTOR BIAS- 2.57E-002 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 6.41E+008 PHOTONS/SEC-CHT2 PC GAIN (Q.E.=0.3)= 7.42E-002(AC) 2.65E-981(DC) SHOT NOISE(Q.E.=0.3)= 2.94E-006 V/HZ11/2 (AC) 5.57E-006 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)- 3.92E-017 W/HZ11/2 (AC) 7.41E-017 W/HZ11/2 (DC) BB TEMP- 58.8 BIAS-0.9498 SIG DEL V-0.91859 DC/1HZ-2.2 BIAS DELTA V-0.0300 NOISE=3.5E-6 BLACKBODY OUTPUT= 1.85E-013 WATTS 3.86E+007 PHOT/SEC SIG. CONDUCTANCE(DC)= 2.82E+802 MHOS/WATT 5.49E-019 MHOS/PHOT/SEC VOLT. RESP. (DC)= 3.16E+011 VOLT/WATT 8.60E-010 VOLT/PHOT/SEC CURR.RESP. (DC)= 6.96E+888 AMP/WATT 1.65E-829 AMP/PHOT/SEC SIG. CONDUCTANCE(1HZ)= 5.51E+001 MHOS/WATT 1.50E-019 MHOS/PHOT/SEC VOLT. RESP.(1HZ)= 9.90E+010 VOLT/WATT 2.60E-010 VOLT/PHOT/SEC CURR.RESP. (1HZ)-1.65E+888 AMP/WATT 4.49E-821 AMP/PHOT/SEC NEP (1HZ)= 3.34E-017 WATT/HZ11/2 1.23E+004 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 3.28E+811 OHMS DETECTOR BIAS- 3.39E-802 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 7.48E+888 PHOTONS/SEC-CHT2 PC GAIN (O.E.=0.3)- 1.83E-881(AC) 3.77E-881(DC) SHOT NOISE(O.E.=0.3)= 4.27E-006 V/HZ11/2 (AC) 8.18E-006 V/HZ11/2 (DC)

SAMPLE NO. GE:GA 3-281-3 RUN DATE 8/9/78 TEMP. =2.5 K

BLIP NEP (Q.E.=0.3)- 4.31E-817 W/HZ11/2 (AC) 8.26E-817 W/HZ11/2 (DC)

OUAN. EFFIC. IF BLIP- 5.88E-801 (AC) 1.83E+800 (DC)

SAMPLE NO. GE: GA 3-2B1-3 **RUN DATE 6/9/78** BB INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-009 LOAD= 7.99E+010

TEMP. =2.5 K

BB TEMP= 58.5	BIAS-0.0500
SIG DEL V-0.02050	DC/1HZ=2.2
BLACKBODY OUTPUT=	1.03E-013 WATTS
SIG. CONDUCTANCE(DC)-	1.95E+002 MHOS/WATT
VOLT. RESP. (DC)-	3.99E+011 VOLT/WATT
CURR.RESP. (DC)=	7.49E+000 AMP/WATT
SIG. CONDUCTANCE (1HZ)=	5.48E+881 NHOS/WATT
VOLT. RESP. (1HZ)=	1.25E+011 VOLT/WATT
CURR.RESP.(1HZ)=	2.05E+000 AMP/WATT
DETECTOR RESISTANCE =	3.55E+011 OHMS
DETECTOR BIAS-	4.18E-002 VOLTS

BIAS DELTA V-0.0380 NOISE-UNDEFINEDO 3.79E+007 PHOT/SEC 5.29E-019 NHOS/PHOT/SEC 1.08E-009 VOLT/PHOT/SEC 2.81E-020 AMP/PHOT/SEC 1.47E-019 NHOS/PHOT/SEC 3.40E-010 VOLT/PHOT/SEC 5.57E-021 AMP/PHOT/SEC

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= PC GAIN (0.E.=0.3)= 1.28E-001(AC)

SHOT NOISE(Q.E.=0.3)= 5.22E-006 V/HZ11/2 (AC) BLIP NEP (Q.E.=0.3)- 4.17E-017 W/HZ11/2 (AC)

7.11E+908 PHOTONS/SEC-CMT2 4.89E-991(DC) 9.90E-006 V/HZT1/2 (DC) 7.91E-817 W/HZT1/2 (DC)

BB TEMP- 58.3 SIG DEL V-0.02400 BLACKBODY OUTPUT= SIG. CONDUCTANCE(DC)= 2.44E+082 MHOS/WATT VOLT. RESP. (DC)-CURR.RESP. (DC)= SIG. CONDUCTANCE (11/Z)= 6.42E+881 MHOS/VATT VOLT. RESP. (1HZ)-CURR.RESP. (1HZ)= NEP (1HZ)-

DETECTOR BIAS-

BIAS-0.0600 DC/1HZ=2.2 1.82E-813 WATTS 4.64E+011 VOLT/WATT 1.82E+801 AMP/WATT 1.48E+011 VOLT/WATT 2.79E+000 AMP/WATT 3.13E-817 WATT/HZT1/2 DETECTOR RESISTANCE = 2.33E+011 OHMS 4.62E-002 VOLTS

BIAS DELTA V-0.8428 NOISE-SE-6 3.74E+007 PHOT/SEC 6.61E-019 NHOS/PHOT/SEC 1.26E-989 VOLT/PHOT/SEC 2.78E-829 AMP/PHOT/SEC 1.74E-819 NHOS/PHOT/SEC 4.00E-018 VOLT/PHOT/SEC 7.31E-021 AMP/PHOT/SEC 1.16E+884 PHOT/SEC-HZ11/2

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= PC GAIN (Q.E.=0.3)= 1.67E-001(AC) SHOT NOISE(Q.E.=0.3)- 7.13E-006 V/HZ11/2 (AC) BLIP NEP (Q.E.=0.3)= 4.83E-017 W/HZT1/2 (AC) 9.42E-017 W/HZT1/2 (DC) QUAN.EFFIC.IF BLIP- 7.13E-001 (AC)

8.64E+008 PHOTONS/SEC-CHT2 6.36E-001(DC) 1.39E-005 V/HZ11/2 (DC) 2.71E+000 (DC)

SAMPLE NO. GE:GA 3-281-3 RUN DATE 6/9/78 TEMP.=2.5 K BB INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-009 LOAD= 7.00E+010

BB TEMP- 58.2 BIAS-8.9688 BIAS DELTA Y-0.8428 SIG DEL V-0.82400 DC/1HZ=2.2 NOISE-UNDEFINEDO BLACKBODY OUTPUT= 1.01E-013 WATTS 3.72E+007 PHOT/SEC SIG. CONDUCTANCE(DC)= 2.46E+882 MHOS/WATT 6.65E-019 MHOS/PHOT/SEC VOLT. RESP. (DC)-4.67E+911 VOLT/WATT 1.26E-009 VOLT/PHOT/SEC CURR.RESP. (DC)= 1.83E+881 AMP/WATT 2.79E-020 AMP/PHOT/SEC SIG. CONDUCTANCE(1HZ)= 6.46E+001 MHOS/WATT 1.75E-019 NHOS/PHOT/SEC VOLT. RESP. (1HZ)-1.49E+011 VOLT/WATT 4.03E-010 VOLT/PHOT/SEC CURR.RESP.(1HZ)= 2.71E+888 AMP/WATT 7.35E-021 AMP/PHOT/SEC DETECTOR RESISTANCE = 2.33E+011 OHMS DETECTOR BIAS-4.62E-002 VOLTS

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA

BACKGROUND PHOTON FLUX DENSITY=

PC GAIN (Q.E.=0.3)= 1.88E-001(AC)

SHOT NOISE(Q.E.=0.3)= 7.15E-006 V/HZT1/2 (AC)

BLIP NEP (Q.E.=0.3)= 4.81E-017 W/HZT1/2 (AC)

9.39E-017 W/HZT1/2 (DC)

BB TEMP- 58.2 BIAS-0.0700 BIAS DELTA V-0.0480 DC/1HZ=2.2 SIG DEL V-0.02700 NOISE=UNDEFINEDO BLACKBODY OUTPUT= 1.01E-013 WATTS 3.72E+007 PHOT/SEC SIG. CONDUCTANCE(DC)= 2.42E+882 MHCS/WATT 6.55E-019 NHOS/PHOT/SEC VOLT. RESP. (DC)= 5.11E+011 VOLT/WATT 1.38E-909 VOLT/PHOT/SEC CURR.RESP. (DC)= 1.16E+001 AMP/WATT 3.14E-828 AMP/PHOT/SEC SIG. CONDUCTANCE(1HZ)= 6.46E+001 NHOS/WATT 1.75E-019 NHOS/PHOT/SEC VOLT. RESP. (1HZ)-1.66E+011 VOLT/WATT 4.49E-010 VOLT/PHOT/SEC CURR.RESP.(1HZ)= 3.10E+000 AMP/WATT 8.48E-821 AMP/PHOT/SEC DETECTOR RESISTANCE = 2.14E+011 OHMS DETECTOR BIAS-5.27E-002 VOLTS

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 9.51E+008 PHOTONS/SEC-CHT2 PC GAIN (0.E.=0.3)= 1.92E-001(AC) 7.29E-001(DC) SHOT NOISE(0.E.=0.3)= 8.36E-006 V/HZT1/2 (AC) 1.62E-005 V/HZT1/2 (DC) BLIP NEP (0.E.=0.3)= 5.06E-017 W/HZT1/2 (AC) 9.76E-017 W/HZT1/2 (DC)

88 INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-009 LOAD= 7.00E+010 BB TEMP- 58.1 BIAS-0.0600 BIAS DELTA V=0.0530 SIG DEL V-0.03000 DC/1HZ-2.2 NOISE-7E-6
BLACKBODY OUTPUT= 1.00E-013 WATTS 3.70E+007 PHOT/SEC SIG. CONDUCTANCE(DC)= 2.56E+002 MHOS/WATT 6.92E-019 MHOS/PHOT/SEC VOLT. RESP. (DC)= 5.69E+011 VOLT/WATT 1.52E-009 VOLT/PHOT/SEC CURR.RESP. (DC)= 1.35E+801 AMP/VATT 3.67E-829 AMP/PHOT/SEC SIG. CONDUCTANCE(1HZ)= 6.79E+801 MHOS/WATT 1.84E-019 NHOS/PHOT/SEC VOLT. RESP. (1HZ)= 1.84E+811 VOLT/WATT 4.98E-818 VOLT/PHOT/SEC CURR.RESP.(1HZ)= 3.69E+000 AMP/WATT 9.74E-021 AMP/PHOT/SEC NEP (1HZ)= 3.48E-017 WATT/HZ11/2 1.28E+004 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 1.87E+011 OHMS DETECTOR BIAS- 5.82E-982 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 1.83E+889 PHOTONS/SEC-CMT2 PC GAIN (Q.E.=0.3)= 2.23E-001(AC) 8.49E-001(DC) SHOT NOISE(Q.E.=0.3)= 9.77E-006 V/HZ11/2 (AC) 1.90E-005 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)= 5.31E-017 W/HZT1/2 (AC) 1.03E-016 W/HZT1/2 (DC) QUAN.EFFIC.IF BLIP- 6.99E-001 (AC) 2.63E+000 (DC) BB TEMP- 58.1 BIAS-0.0900 BIAS DELTA V-0.0555 SIG DEL V-0.03200 DC/1HZ=2.2 NOISE=UNDEFINED0
BLACKBODY OUTPUT= 1.00E-013 WATTS 3.70E+007 PHOT/SEC SIG. CONDUCTANCE(DC)- 2.87E+882 MHOS/WATT 7.76E-019 MHOS/PHOT/SEC VOLT. RESP. (DC)= 5.76E+811 VOLT/WATT 1.58E-989 VOLT/PHOT/SEC CURR.RESP. (DC)= 1.59E+981 AMP/WATT 4.31E-020 AMP/PHOT/SEC SIG. CONDUCTANCE (1HZ)= 7.47E+901 MHOS/WATT 2.02E-019 NHOS/PHOT/SEC VOLT. RESP. (1HZ)= 1.94E+011 VOLT/WATT 5.25E-818 VOLT/PHOT/SEC CURR.RESP.(1HZ)= 4.15E+000 AMP/WATT 1.12E-020 AMP/PHOT/SEC DETECTOR RESISTANCE = 1.47E+011 OHMS DETECTOR BIAS-6.19E-002 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA PC GAIN (Q.E.=0.3)= 2.57E-001(AC) 1.17E+009 PHOTONS/SEC-CMT2 9.86E-001(DC) SHOT NOISE(Q.E.=0.3)= 1.13E-005 V/HZ11/2 (AC) 2.21E-005 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)= 5.81E-817 W/HZT1/2 (AC) 1.14E-916 W/HZT1/2 (DC)

RUN DATE 6/9/78 TEMP. = 2.5 K

SAMPLE NO. GE:GA 3-2B1-3

SAMPLE NO. GE:GA 3-281-3 RUN DATE 6/9/78 TEMP.=2.5 K

88 INTEGRATED FROM 48 TO 138 MICRONS STEP 8.2

ETENDUE= 8.84E-889 LOAD= 7.88E+818

BIAS-0.1999 BIAS DELTA V-9.9589 BB TEMP- SB. 1 DC/1HZ=2.2 SIG DEL V-0.83480 NOISE=9E-6 BLACKBODY OUTPUT= 1.99E-013 WATTS 3.79E+997 PHOT/SEC 8.58E-819 MHOS/PHOT/SEC SIG. CONDUCTANCE(DC)= 3.17E+882 MHOS/WATT 1.61E-000 VOLT/PHOT/SEC 5.95E+011 VOLT/WATT VOLT. RESP. (DC)-4.96E-829 AMP/PHOT/SEC 1.84E+001 AMP/WATT CURR.RESP. (DC)= 2.29E-819 NHOS/PHOT/SEC SIG. CONDUCTANCE (1HZ) = 8.13E+881 NHOS/WATT 5.53E-010 VOLT/PHOT/SEC YOLT. RESP. (1HZ)-2.84E+811 VOLT/WATT CURR.RESP. (1HZ)= 4.71E+000 AMP/WATT 1.28E-020 AMP/PHOT/SEC 3.89E-817 WATT/HZT1/2 1.44E+884 PHOT/SEC-HZ11/2 NEP (1HZ)= DETECTOR RESISTANCE = 1.23E+011 OHMS DETECTOR BIAS-6.37E-992 VOLTS

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA
BACKGROUND PHOTON FLUX DENSITY= 1.26E+889 PHOTONS/SEC-CNT2
PC GAIN (Q.E.=0.3)= 2.92E-801 (AC) 1.14E+890 (DC)
SHOT NOISE(Q.E.=0.3)= 1.26E-895 V/HZT1/2 (AC) 2.58E-895 V/HZT1/2 (DC)
BLIP NEP (Q.E.=0.3)= 6.19E-917 W/HZT1/2 (AC) 1.22E-816 W/HZT1/2 (DC)
QUAN.EFFIC.IF BLIP= 7.58E-881 (AC) 2.95E+898 (DC)

TEMP.=3 K SAMPLE NO. GE:GA 4-581-1 RUN DATE 7/11/78
BB INTEGRATED FROM 49 TO 199 MICRONS STEP 9.2 ETENDUE= 6.84E-009 LOAD= 5.80E+010 BB TEMP= 58.1 BIAS=0.9959 SIG DEL V=0.99998 DC/1HZ=1.94 BLACKBODY OUTPUT= 1.99E-913 WATTS BIAS DELTA V-0.9997 NOISE-UNDEFINEDO 3.70E+007 PHOT/SEC SIG. CONDUCTANCE(DC)- 1.56E+882 MHOS/WATT

4.22E-019 NHOS/PHOT/SEC VOLT. RESP. (DC)= 8.37E+888 VOLT/WATT
CURR.RESP. (DC)= 1.89E-881 ANP/WATT 2.27E-812 VOLT/PHOT/SEC CURR. RESP. (DC)-1.09E-001 AMP/WATT 2.95E-022 AMP/PHOT/SEC SIG. CONDUCTANCE (1HZ)= 1.49E+002 MHOS/WATT 4.84E-019 MHOS/PHOT/SEC 8.04E+008 VOLT/HATT VOLT. RESP. (1HZ)-2.18E-012 VOLT/PHOT/SEC 1.04E-001 AMP/WATT CURR. RESP. (1HZ)= 2.83E-022 AMP/PHOT/SEC DETECTOR RESISTANCE = 9.89E+889 OHMS DETECTOR BIAS-7.69E-004 VOLTS

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= PC GAIN-6.47E-003(AC)

1.31E-007 V/HZT1/2 (AC) 1.34E-007 V/HZT1/2 (DC) SHOT NOISE -

BLIP NEP-1.63E-816 W/HZT1/2 (AC) 1.67E-816 W/HZT1/2 (DC)

BIAS-0.9199 BB TEMP- 59.8 SIG DEL V-0.88818 BLACKBODY OUTPUT= DC/1HZ=1.84 1.12E-013 WATTS SIG. CONDUCTANCE(DC)= 2.39E+882 MHOS/WATT VOLT. RESP. (DC)= 1.69E+889 VOLT/NATT
CURR.RESP. (DC)= 2.67E-881 AMP/NATT 2.87E-001 AMP/WATT SIG. CONDUCTANCE (1HZ)= 2.29E+882 MHOS/WATT 1.73E+889 VOLT/WATT VOLT. RESP. (1HZ)= CURR. RESP. (1HZ)= 2.74E-001 AMP/WATT DETECTOR RESISTANCE = 7.59E+889 CHHS DETECTOR BIAS-1.32E-003 VOLTS

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= PC GAIN-

1.72E-882(AC) 1.88E-882(DC)
2.82E-887 V/HZT1/2 (AC) 2.88E-887 V/HZT1/2 (DC)
1.51E-816 V/HZT1/2 (AC) 1.55E-816 W/HZT1/2 (DC) SHOT NOISE =

3.46E+818 PHOTONS/SEC-CMT2 6.76E-003(DC)

BIAS DELTA V-0.8012 NOISE=UNDEFINEDO 4.00E+007 PHOT/SEC 6.54E-019 NHOS/PHOT/SEC 4.93E-912 VOLT/PHOT/SEC 7.85E-022 AMP/PHOT/SEC 6.25E-019 NHOS/PHOT/SEC 4.74E-012 VOLT/PHOT/SEC 7.58E-822 AMP/PHOT/SEC

2.68E+010 PHOTONS/SEC-CHT2

BB INTEGRATED FROM 48 TO 138 MICRONS STEP 8.2 ETENDUE- 6.84E-009 LOAD= 5.88E+818 BIAS DELTA V-9.9826 BB TEMP- 60.8 BIAS-0.0200 SIG DEL V-0.00038 1.13E-813 VATTS A 14F-006-6 BLACKBODY OUTPUT= 4.14E+007 PHOT/SEC SIG. CONDUCTANCE(DC)= 2.87E+882 HHOS/WATT 5.65E-019 NHOS/PHOT/SEC VOLT. RESP. (DC)- 3.72E+889 VOLT/WATT 1.82E-811 VOLT/PHOT/SEC CURR.RESP. (DC)= 5.39E-001 AMP/WATT 1.48E-021 AMP/PHOT/SEC SIG.CONDUCTANCE(1HZ)= 1.97E+882 MHOS/WATT 5.48E-819 MHOS/PHOT/SEC VOLT. RESP.(1HZ)= 3.57E+889 VOLT/WATT 9.77E-812 VOLT/PHOT/SEC CURR.RESP.(1HZ)= 5.15E-881 AMP/WATT 1.41E-821 AMP/PHOT/SEC NEP (IHZ)-8.48E-816 WATT/HZT1/2 2.34E+885 PHOT/SEC-HZT1/2 DETECTOR RESISTANCE = 8.37E+009 OHMS DETECTOR BIAS-2.67E-003 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 2.82E+010 PHOTONS/SEC-CMT2 PC GAIN (0.E.=0.3)= 3.23E-002(AC) 3.38E-002(DC) SHOT NOISE(Q.E.=0.3)= 5.49E-007 V/HZ+1/2 (AC) 5.62E-007 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)= 1.54E-016 W/HZ11/2 (AC) 1.57E-016 W/HZT1/2 (DC) BLIP QUAN EFFIC = 1.73E-002 (AC) 1.81E-902 (DC) 88 TEMP- 89.2 BIAS-0.0300 BIAS DELTA V-0.0049 SIG DEL V-9.99984 BLACKBODY GUTPUT-DC/1HZ=1.84 NOTSE=3.2E-6 1.15E-013 WATTS SIG. CONDUCTANCE(DC)= 2.81E+882 MHOS/WATT
VOLT. RESP. (DC)= 8.31E+889 VOLT/WATT BLACKBODY OUTPUT-4.19E+007 PHOT/SEC 5.51E-019 NHOS/PHOT/SEC 2.27E-011 VOLT/PHOT/SEC VOLT. RESP. (DC)= 9.85E-801 AMP/WATT
SIG. CONDUCTANCE (1HZ)= 1.92E+802 MHOS/WATT
VOLT. RESP. (1HZ)= 7.96E+809 VOLT/WATT
CURR. RESP. (1HZ)= 9.40E-801 AMP/WATT 2.70E-021 AMP/PHOT/SEC 5.25E-019 NHOS/PHOT/SEC 2.18E-011 VOLT/PHOT/SEC 2.57E-021 AMP/PHOT/SEC NEP (1HZ)-3.45E-016 WATT/HZT1/2 1.26E+005 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 1.89E+818 CHMS DETECTOR BIAS- 5.38E-003 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 2.21E+018 PHOTONS/SEC-CHT2 PC GAIN (Q.E.=Q.3)- 5.69E-802(AC) 6.16E-002(DC) SHOT NOISE(O.E.-0.3)- 1.11E-006 V/HZ11/2 (AC) 1.14E-996 V/HZT1/2 (DC) BLIP NEP (Q.E.=0.3)- 1.39E-816 W/HZT1/2 (AC) 1.43E-816 W/HZT1/2 (DC) BLIP QUAN.EFFIC.= 4.99E-882 (AC) 5.13E-882 (DC)

RUN DATE 7/11/78 TEMP.=3 K

SAMPLE NO. GE:GA 4-581-1

The state of the s

the state of the s

SAMPLE NO. GE:GA 4-581-1 RUN DATE 7/11/78 TEMP.=3 K
BB INTEGRATED FROM 48 TO 138 MICRONS STEP 8.2 ETENDUE = 6.84E-888 LOAD- 5.88E+818 BB TEMP- 60.3 BIAS-0.0400 BIAS DELTA V-8.9968 SIG DEL V-0.80120 DC/1HZ=1.84 NOISE=4E-6
BLACKBODY OUTPUT= 1.15E-013 WATTS 4.21E+007 P 4.21E+007 PHOT/SEC SIG.CONDUCTANCE(DC)= 2.01E+002 MHOS/WATT

VOLT. RESP.(DC)= 1.16E+010 VOLT/WATT

CURR.RESP.(DC)= 1.36E+000 AMP/WATT

SIG.CONDUCTANCE(1HZ)= 1.91E+002 MHOS/WATT

VOLT. RESP.(1HZ)= 1.15E+010 VOLT/WATT

CURR.RESP.(1HZ)= 1.30E+000 AMP/WATT 5.58E-019 MHOS/PHOT/SEC 3.24E-011 VOLT/PHOT/SEC 3.72E-021 AMP/PHOT/SEC 5.25E-019 MHOS/PHOT/SEC 3.11E-011 VOLT/PHOT/SEC 3.55E-021 AMP/PHOT/SEC 3.82E-016 WATT/HZT1/2 NEP (1HZ)-1.18E+805 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 1.14E+010 OHMS DETECTOR BIAS-7.44E-883 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY=
PC GAIN (Q.E.=0.3)= 8.13E-002(AC) BACKGROUND PHOTON FLUX DENSITY= 2.12E+818 PHOTONS/SEC-CHT2 6.53E-002(DC) SHOT NOISE(Q.E.=0.3)= 1.56E-006 V/HZT1/2 (AC) 1.60E-006 V/HZT1/2 (DC) BLIP NEP (Q.E.=8.3)= 1.37E-016 W/HZT1/2 (AC) 1.41E-016 W/HZT1/2 (DC)
QUAN.EFFIC.IF BLIP= 6.29E-002 (AC) 6.50E-002 (DC) 88 TEMP- 60.4 BIAS-0.0500 BIAS DELTA V-0.0083 SIG DEL V-0.88141 DC/1HZ=1.84 NOISE=5.1E-6 BLACKBODY OUTPUT= 1.16E-013 VATTS 4.24E+007 PHOT/SEC SIG.CONDUCTANCE(DC)= 1.93E+882 NHOS/WATT 5.38E-818 NHOS/PHOT/SEC VOLT. RESP.(DC)= 1.38E+818 VOLT/WATT 3.78E-811 VOLT/PHOT/SEC CURR.RESP.(DC)= 1.69E+888 AMP/WATT 4.48E-821 AMP/PHOT/SEC SIG.CONDUCTANCE(1HZ)- 1.84E+882 NHOS/WATT 5.85E-819 MHOS/PHOT/SEC VOLT. RESP.(1HZ)= 1.32E+010 VOLT/WATT CURR.RESP.(1HZ)= 1.53E+000 AMP/WATT 3.63E-011 VOLT/PHOT/SEC 4.19E-021 AMP/PHOT/SEC NEP (1HZ)= 3.33E-016 WATT/HZT1/2 1.21E+006 PHOT/SEC-HZT1/2 DETECTOR RESISTANCE = 1.12E+819 OHMS DETECTOR BIAS-9.12E-003 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 2.26E+019 PHOTONS/SEC-CHT2 PC GAIN (Q.E.-0.3)- 9.50E-802(AC)

SHOT NOISE(0.E.=0.3)- 1.86E-886 V/HZ11/2 (AC) 1.98E-886 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)- 1.41E-016 W/HZT1/2 (AC) 1.44E-016 W/HZT1/2 (DC)

QUAN EFFIC. IF BLIP- 5.57E-002 (AC)

1:81E-801C DC)

5.63E-002 (DC)

SAMPLE NO. GE:GA 4-581-1 RUN DATE 7/11/78 TEMP.=3 K BB INTEGRATED FROM 40 TO 130 NICRONS STEP 0.2 ETENDUE = 6.84E-009 LOAD- 5.88E+818

SIG DEL V=0.80172 DC/1HZ=1.84
BLACKBODY OUTPUT= 1.18F_010 BIAS DELTA V-0.0100 NOISE-UNDEFINEDO 1.18E-013 WATTS 4.31E+007 PHOT/SEC SIG. CONDUCTANCE(DC)- 1.94E+882 MHOS/WATT 5.32E-819 MHOS/PHOT/SEC VOLT. RESP. (DC)= 1.86E+818 VOLT/WATT 4.53E-811 VOLT/PHOT/SEC CURR.RESP. (DC)= 1.93E+800 AMP/WATT 5.38E-821 AMP/PHOT/SEC SIG.CONDUCTANCE(1HZ)= 1.86E+802 MHOS/WATT 5.86E-819 MHOS/PHOT/SEC VOLT. RESP. (1HZ)= 1.58E+010 VOLT/WATT 4.3SE-011 VOLT/PHOT/SEC CURR.RESP. (1HZ)= 1.84E+000 AMP/WATT 5.0SE-021 AMP/PHOT/SEC DETECTOR RESISTANCE = 1.11E+010 OHMS 1.99E-982 VOLTS DETECTOR BIAS-

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= PC GAIN (0.E.=0.3)= 1.16E-801(AC) SHOT NOISE(Q.E.=0.3)= 2.23E-806 V/HZT1/2 (AC)

2.25E+818 PHOTONS/SEC-CHT2 THOSE ABOVE 1.21E-001(DC) 2.29E-806 V/HZT1/2 (DC) BLTP NEP (Q.E.=0.3)- 1.41E-016 W/HZT1/2 (AC) 1.44E-016 W/HZT1/2 (DC)

58 TEIP- 50.7 BIAS-0.0700 SIG DEL V-0.00202 DC/1HZ=1.84 BLACKBODY OUTPUT= 1.16E-013 WATTS
SIG.CONDUCTANCE(DC)= 1.82E+892 MHOS/WATT
VOLT. RESP.(DC)= 1.94E+018 VOLT/WATT
CURR.RESP.(DC)= 2.18E+899 AMP/WATT SIG. CONDUCTANCE (1HZ)- 1.73E+882 HHOS/WATT VOLT. RESP. (1HZ)- 1.86E+018 VOLT/WATT CLRR. RESP. (1HZ)-2.95E+989 AMP/WATT NEP (IHZ)= 2.69E-016 WATT/HZT1/2 DETECTOR RESISTANCE = 1.16E+010 OHMS DETECTOR BIAS- 1.32E-002 VOLTS

BIAS DELTA V-0.0120 NOISE=5.8E-6 4.31E+007 PHOT/SEC 4.99E-819 NHOS/PHOT/SEC 5.32E-011 VOLT/PHOT/SEC 5.99E-821 AMP/PHOT/SEC 4.76E-819 NHOS/PHOT/SEC 5.11E-011 VOLT/PHOT/SEC 5.71E-821 AMP/PHOT/SEC 9.81E+804 PHOT/SEC-HZ11/2

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= PC GAIN (Q.E.=0.3)= 1.31E-001(AC) 1.37E-001(DC) SHOT NOISE(O.E.=0.3)= 2.64E-896 V/HZ11/2 (AC) 2.71E-896 V/HZ11/2 (DC) BLTP NEP (0.E.=0.3)- 1.42E-016 W/HZT1/2 (AC) 1.45E-016 W/HZT1/2 (DC) DUAN EFFIC. IF BLIP- 8.33E-882 (AC) COO) STITIFFY BIS-384 1 (CA) STITIFFY BIS-315 1 -(8-8-815 WALTING COC)

2.30E+010 PHOTONS/SEC-CNT2 6.74E-982 (DC)

SAMPLE NO. GE:GA 4-581-1 RUN DATE 7/11/78 TEMP.=3 K
BB INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-009 LOAD= 5.98E+010 BB TEMP- 60.6 BIAS-0.0800 BIAS DELTA V-0.0138 DC/1HZ=1 SIG DEL V-0.00238 NOISE=6.7E-6 BLACKBODY OUTPUT= 1.18E-013 WATTS 4.26E+007 PHOT/SEC SIG.CONDUCTANCE(DC)= 1.87E+002 MHOS/WATT 5.13E-019 MHOS/PHOT/SEC VOLT. RESP.(DC)= 2.30E+010 VOLT/WATT 6.31E-011 VOLT/PHOT/SEC CURR.RESP.(DC)= 2.58E+000 AMP/WATT 7.06E-021 AMP/PMOT/SEC SIG. CONDUCTANCE (1HZ)- 1.87E+882 MHOS/WATT 5.15E-619 MHOS/PHOT/SEC 2.38E+010 VOLT/WATT 6.31E-011 VOLT/PHOT/SEC 2.58E+000 AMP/WATT 7.98E-021 AMP/PHOT/SEC VOLT. RESP. (1HZ)= CURR.RESP. (1HZ)-NEP (1HZ)= 2.49E-016 WATT/HZT1/2 9.96E+004 PHOT/SEC-HZT1/2 DETECTOR RESISTANCE = 1.17E+010 OHMS DETECTOR BIAS-1.52E-002 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 2.22E+818 PHOTONS/SEC-CHT2 PC GAIN (Q.E.=0.3)= 1.62E-001(AC) 1.62E-001(DC) SHOT NOISE(Q.E.=8.3)= 3.16E-886 V/HZ11/2 (AC) 3.16E-886 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)= 1.38E-016 W/HZT1/2 (AC) 1.38E-016 W/HZT1/2 (DC) QUAN EFFIC IF BLIP- 9.14E-002 (AC) 9.14E-002 (DC) BB TEMP- 60.4 BIAS-0.8980 SIG DEL V-0.88269 DC/1HZ=1 BIAS DELTA V-0.0162 SIG DEL V-0.00260 NOISE=8.5E-6 BLACKBODY OUTPUT= 1.16E-013 WATTS 4.24E+997 PHOT/SEC SIG.CONDUCTANCE(DC)= 1.88E+882 HHOS/WATT 4.58E-819 HHOS/PHOT/SEC VOLT. RESP. (DC) = 2.54E+010 VOLT/WATT 6.97E-011 VOLT/PHOT/SEC CURR.RESP. (DC) = 2.79E+000 AMP/WATT 7.39E-021 AMP/PHOT/SEC SIG.CONDUCTANCE(1HZ)= 1.86E+882 MHOS/WATT 4.56E-019 NHOS/PHOT/SEC 2.54E+010 VOLT/WATT 6.97E-011 VOLT/PHOT/SEC 2.79E+000 AMP/WATT 7.39E-021 AMP/PHOT/SEC VOLT. RESP. (1HZ)= CURR.RESP. (1HZ)= NEP (IHZ)= 2.99E-016 WATT/HZT1/2 1.96E+006 PHOT/SEC-HZT1/2 DETECTOR RESISTANCE = 1.29E+018 OHMS DETECTOR BIAS-1.76E-002 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 2.37E+818 PHOTONS/SEC-CHT2
PC GAIN (0.E.=0.3)= 1.69E-801(AC) 1.69E-801(DC) SHOT NOISE(Q.E.=0.3)= 3.56E-006 V/HZ11/2 (AC) 3.56E-006 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)- 1.48E-016 W/HZT1/2 (AC) 1.48E-016 W/HZT1/2 (DC)

QUAN EFFIC IF BLIP- 7.00E-002 (AC) 7.00E-002 (DC)

RUN DATE 7/11/78 TEMP.=3 K BB INTEGRATED FROM 48 TO 138 MICRONS STEP 9.2 ETENDUE= 6.84E-009 LOAD= 5.00E+018 SIS DEL V-0.80245 DC/1HZ=1 BIAS DELTA V-0.8152 NOISE=9E-6 4.24E+007 PHOT/SEC BLACKBODY OUTPUT= 1.16E-013 WATTS SIG.CONDUCTANCE(DC)= 1.98E+092 MHOS/WATT 5.49E-019 MHOS/PHOT/SEC VOLT. RESP.(DC)= 2.38E+010 VOLT/WATT 6.53E-011 VOLT/PHOT/SEC CURR.RESP. (DC)= 3.81E+888 AMP/WATT 8.28E-821 AMP/PHOT/SEC SIG.CONDUCTANCE(1HZ)= 1.98E+882 MHOS/WATT 5.43E-819 MHOS/PHOT/SEC VOLT. RESP.(1HZ)= 2.38E+818 VOLT/WATT 6.53E-811 VOLT/PHOT/SEC CURR.RESP.(1HZ)= 3.81E+888 AMP/WATT 8.28E-821 AMP/PHOT/SEC NEP (1HZ)= 3.26E-816 VATT/HZ11/2 1.19E+885 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 1.00E+010 OHMS DETECTOR BIAS-1.67E-002 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 2.45E+010 PHOTONS/SEC-CHT2 1.89E-001(DC) PC GAIN (Q.E.=0.3)= 1.69E-001(AC) SHOT NOISE(0.E.=0.3)= 3.41E-006 V/HZ11/2 (AC) 3.41E-006 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)= 1.49E-016 W/HZ11/2 (AC) 1.49E-016 W/HZ11/2 (DC) QUAN. EFFIC. IF BLIP- 5.89E-892 (AC) 5.88E-882 (DC) BB TEMP= 80.4 BIAS=0.2000 BIAS DELTA V=0.0286 SIG DEL V=0.00385 DC/1HZ=.9 NGISE=1.8E=5. BLACKBODY OUTPUT= 1.16E=013 WATTS 4.24E+007 PHOT/SEC BIAS DELTA V-0.0286 SIG.CONDUCTANCE(DC)= 1.71E+882 NHOS/WATT 4.67E-819 NHOS/PHOT/SEC VOLT. RESP. (DC)= 3.72E+010 VOLT/WATT 1.02E-010 VOLT/PHOT/SEC CURR.RESP. (DC)= 4.88E+888 AMP/WATT SIG. CONDUCTANCE(1HZ)= 1.93E+882 MHOS/WATT 1.34E-828 AMP/PHOT/SEC 5.28E-019 NHOS/PHOT/SEC VOLT. RESP. (1HZ)= 4.15E+818 VOLT/WATT 1.14E-010 VOLT/PHOT/SEC CURR. RESP. (1HZ)= 5.51E+000 AMP/WATT 1.51E-020 AMP/PHOT/SEC NEP (1HZ)= 3.78E-016 WATT/HZT1/2 1.36E+005 PHOT/SEC-HZT1/2 DETECTOR RESISTANCE = 9.32E+009 OHMS DETECTOR BIAS- 3.14E-002 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY=
PC GAIN (Q.E.-0.3)- 3.46E-001 (AC) 3.86E+818 PHOTONS/SEC-CMT2 3.96E-001(DC) SHOT NOISE(Q.E.=0.3)- 6.18E-886 V/HZT1/2 (AC) 5.81E-886 V/HZT1/2 (DC)

SAMPLE NO. GE:GA 4-581-1

BLIP NEP (Q.E.=Q.3)- 1.49E-Q16 V/HZT1/2 (AC) 1.49E-Q16 V/HZT1/2 (DC) QUAN . EFFIC . IF BLIP- 4.86E-882 (AC) 4.12E-882 (DC)

SAMPLE NO. GE: GA 4-581-1 RUN DATE 7/11/78 TEMP. =3 K BB INTEGRATED FROM 48 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-009 LOAD= 5.00E+010 BIAS-0.3000 BB TEMP- 60.4 BIAS DELTA V-0.0378 SIG DEL V-0.00425 DC/1HZ=.9 NOISE=2E-5 1.16E-013 WATTS BLACKBODY OUTPUT= 4.24E+007 PHOT/SEC SIG. CONDUCTANCE(DC)= 1.58E+002 NHOS/WATT 4.32E-019 NHOS/PHOT/SEC VOLT. RESP. (DC)= 4.89E+818 VOLT/WATT 1.12E-010 VOLT/PHOT/SEC CURR.RESP. (DC)= 5.96E+000 AMP/WATT 1.63E-020 AMP/PHOT/SEC SIG. CONDUCTANCE (1HZ) = 1.78E+802 NHOS/WATT 4.87E-019 NHOS/PHOT/SEC 4.55E+010 VOLT/WATT VOLT. RESP. (1HZ)-1.25E-010 VOLT/PHOT/SEC CURR.RESP. (1HZ)= 6.71E+000 AMP/WATT 1.84E-820 AMP/PHOT/SEC 3.92E-016 VATT/HZ11/2 NEP (1HZ)= 1.43E+805 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 8.04E+009 OHMS 4.15E-002 VOLTS DETECTOR BIAS-THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 3.84E+010 PHOTONS/SEC-CMT2 PC GAIN (0.E.=0.3)= 4.21E-001(AC) 3.74E-001(DC) SHOT NOISE(D.E.=0.3)= 7.44E-006 V/HZT1/2 (AC) 7.01E-006 V/HZT1/2 (DC) BLIP NEP (Q.E.=0.3)= 1.64E-016 W/HZ11/2 (AC) 1.54E-016 W/HZ11/2 (DC) QUAN. EFFIC. IF BLIP- 5.23E-002 (AC) 4.64E-002 (DC) 88 TEMP- 60.3 BIAS-0.4000 BIAS DELTA V-0.0456 SIG DEL V-8.88475 DC/1HZ=.9 NOISE=2.1E-5 1.15E-013 WATTS BLACKSODY OUTPUT= 4.21E+007 PHOT/SEC STE TOPOUCTANCE (DC)= 1.61E+882 NHOS/WATT 4.41E-019 NHOS/PHOT/SEC VALTE RESP. (DC)= 4.58E+010 VOLT/WATT 1.26E-010 VOLT/PHOT/SEC 7.34E+000 AMP/WATT 2.81E-828 AMP/PHOT/SEC SIG. CONDUCTANCE (1HZ)= 1.81E+002 NHOS/WATT 4.96E-019 NHOS/PHOT/SEC 1.48E-010 VOLT/PHOT/SEC VOLT. RESP. (1HZ)= 5.19E+019 VOLT/WATT 2.25E-829 AMP/PHOT/SEC CURR.RESP.(1HZ)= 8.26E+000 AMP/WATT NEP (IHZ)-3.69E-016 WATT/HZT1/2 1.35E+005 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 7.16E+009 OHMS DETECTOR BIAS-5.01E-002 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA

SHOT NOISE(Q.E.=0.3)= 8.68E-896 V/HZ11/2 (AC) 8.18E-896 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)= 1.78E-816 W/HZ11/2 (AC) 1.68E-816 W/HZ11/2 (DC)

4.22E+010 PHOTONS/SEC-CHT2

4.60E-001(DC)

5.66E-902 (DC)

BACKGROUND PHOTON FLUX DENSITY=

PC GAIN (Q.E.=0.3)= 5.18E-801(AC)

QUAN.EFFIC.IF BLIP- 6.37E-002 (AC)

SAMPLE NO. GE:GA 4-581-1 RUN DATE 7/11/78 BB INTEGRATED FROM 48 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-889 LOAD= 5.88E+818

TEMP.=3 K

BIAS DELTA V-0.0529 BB TEMP- 68.3 BIAS-0.5000 SIG DEL V-0.88578 DC/1HZ=.9 NOISE=2.2E-5 BLACKBODY OUTPUT= 1.15E-013 WATTS 4.21E+967 PHOT/SEC 5.12E-819 MHOS/PHOT/SEC SIG. CONDUCTANCE(DC)= 1.87E+882 NHOS/WATT VOLT. RESP. (DC)-5.50E+010 VOLT/WATT 1.51E-010 VOLT/PHOT/SEC CURR.RESP. (DC)= 9.71E+000 AMP/WATT 2.65E-020 AMP/PHOT/SEC SIG. CONDUCTANCE(1HZ)= 2.19E+862 NHOS/VATT 5.76E-019 NHOS/PHOT/SEC VOLT. RESP. (1HZ)= 6.12E+019 VOLT/WATT 1.68E-019 VOLT/PHOT/SEC 3.00E-020 AMP/PHOT/SEC CURR.RESP. (1HZ)-1.89E+881 AMP/WATT 1.17E+005 PHOT/SEC-HZ11/2 NEP (1HZ)-3.20E-016 VATT/HZ11/2 DETECTOR RESISTANCE = 6.45E+889 OHMS 5.71E-002 VOLTS DETECTOR BIAS-

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY=
PC GAIN (Q.E.=0.3)= 5.88E-801(AC)
SHOT NOISE(Q.E.=0.3)= 1.88E-806 V/HZ11/2 (AC)
BLIP NEP (Q.E.=0.3)= 1.68E-816 W/HZ11/2 (AC)
OUAN.EFFIC.IF BLIP= 8.22E-882 (AC)

4.84E+018 PHOTONS/SEC-CHT2 6.89E-801(DC) 9.66E-806 V/HZT1/2 (DC) 1.58E-816 W/HZT1/2 (DC) 7.29E-802 (DC)

SAMPLE NO. GE:GA 4-681-1 RUN DATE 7/11/78 TEMP.=2.5 K 88 INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-009 LOAD= 7.00E+010 88 TEMP- 59.7 BIAS=0.0050 DC/1HZ=4.7 BIAS DELTA V-0.0043 1.11E-013 WATTS 4 07E-009 SIG DEL V-0.00148 SIG. CONDUCTANCE(DC)= 7.14E+801 NHOS/WATT 1.95E-019 NHOS/PHOT/SEC VOLT. RESP. (DC)= 2.17E+818 VOLT/WATT 5.93E-011 VOLT/PHOT/SEC CURR.RESP. (DC)= 3.07E-001 AMP/WATT 8.20E-022 AMP/WATT CURR.RESP. (DC)= 3.07E-001 AMP/WATT 8.39E-022 AMP/PHOT/SEC SIG.CONDUCTANCE(1HZ)= 1.08E+001 MHOS/WATT 2.94E-020 MHOS/PHOT/SEC VOLT. RESP.(1HZ)= 3.35E+889 VOLT/WATT 9.14E-812 VOLT/PHOT/SEC CURR.RESP.(1HZ)= 4.62E-882 AMP/WATT 1.26E-822 AMP/PHOT/SEC CURR.RESP.(1HZ)= NEP (1HZ)= 5.65E-016 WATT/HZ11/2 2.87E+005 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 1.20E+012 OHMS DETECTOR BIAS-4.73E-003 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 5.68E+008 PHOTONS/SEC-CMT2 PC GAIN (Q.E.=0.3)= 2.89E-003(AC) 1.92E-002(DC) SHOT NOISE(O.E.=0.3)- 1.62E-887 V/HZT1/2 (AC) 4.18E-887 V/HZT1/2 (DC) BLIP NEP (Q.E.=0.3)- 4.85E-017 W/HZ11/2 (AC) 1.25E-016 W/HZ11/2 (DC) OUAN.EFFIC.IF BLIP- 2.21E-903 (AC) 1.46E-982 (DC) SIG DEL V-0.98390 DC/1HZ-4.7
BLACKBODY OUTPUT= 1.19F-819 1/4 BIAS DELTA V-0.0087 NOISE-1.9E-6 1.10E-013 WATTS 4.84E+887 PHOT/SEC SIG.CONDUCTANCE(DC)= 7.14E+801 MHOS/VATT
VOLT. RESP.(DC)= 4.45E+818 VOLT/VATT
CURR.RESP.(DC)= 6.21E-801 AMP/VATT 1.95E-019 NHOS/PHOT/SEC 1.22E-010 VOLT/PHOT/SEC 1.69E-021 AMP/PHOT/SEC 2.93E-020 NHOS/PHOT/SEC 1.87E-011 VOLT/PHOT/SEC CURR.RESP.(1HZ)= NEP (1HZ)= 2.55E-022 AMP/PHOT/SEC 2.77E-016 WATT/HZT1/2 1.82E+905 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 1.48E+012 OHMS DETECTOR BIAS-9.55E-003 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 4.61E+008 PHOTONS/SEC-CMT2 PC GAIN (Q.E.=0.3)= 5.83E-083(AC) 3.88E-982(DC) SHOT NOISE(O.E.=0.3)= 2.98E-907 V/HZ11/2 (AC) 7.69E-907 V/HZ11/2 (DC)

BLIP NEP (Q.E.=0.3)= 4.38E-017 W/HZT1/2 (AC) 1.13E-016 W/HZT1/2 (DC)
QUAN.EFFIC.IF BLIP= 7.44E-003 (AC) 4.95E-002 (DC)

SAMPLE NO. GE:GA 4-5B1-1 RUN DATE 7/11/78 TEMP. = 2.5 K BB INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-009 LOAD= 7.00E+010 BIAS-0.0290 BB TEMP- 59.4 BIAS DELTA V-0.0168 SIG DEL V-0.99699 DC/1HZ=4.8 NOISE=1.8E-6 1.09E-013 WATTS BLACKBODY OUTPUT= 4.00E+007 PHOT/SEC SIG. CONDUCTANCE(DC)= 7.89E+801 MHOS/WATT 2.15E-019 MHOS/PHOT/SEC VOLT. RESP. (DC)-9.02E+010 VOLT/WATT 2.46E-010 VOLT/PHOT/SEC CURR.RESP. (DC)= 1.33E+000 AMP/WATT 3.61E-021 AMP/PHOT/SEC SIG. CONDUCTANCE (1HZ)= 1.14E+801 MHOS/VATT 3.11E-020 MHOS/PHOT/SEC VOLT. RESP. (1HZ)= 1.35E+010 VOLT/WATT 3.69E-011 VOLT/PHOT/SEC 1.92E-001 AMP/WATT CURR. RESP. (1HZ)-5.29E-022 AMP/PHOT/SEC NEP (1HZ)-1.32E-016 WATT/HZ11/2 4.85E+904 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 8.49E+811 OHMS DETECTOR BIAS-1.85E-992 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 7.38E+008 PHOTONS/SEC-CMT2 PC GAIN (Q.E.=0.3)= 1.29E-902(AC) 8.27E-002(DC) SHOT NOISE(Q.E.=0.3)= 7.63E-907 Y/HZ11/2 (AC) 2.01E-906 Y/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)- 5.64E-017 W/HZT1/2 (AC) 1.48E-016 W/HZT1/2 (DC) QUAN. EFFIC. IF BLIP- 5.46E-002 (AC) 3.77E-001 (DC) BB TEMP- 59.9 BIAS-0.0400 BIAS DELTA V-8.0337 SIG DEL V-0.01400 DC/1HZ=4.8 NOTSE=1.9E-6 BLACKBODY OUTPUT= 1.06E-013 WATTS 3.90E+007 PHOT/SEC SIG. CONDUCTANCE(DC)= 1.83E+882 NHOS/WATT 2.81E-019 NHOS/PHUT/SEC VOLT. RESP. (DC)= 2.35E+011 VOLT/WATT 6.40E-010 VOLT/PHOT/SEC CURR.RESP. (DC)= 3.48E+000 AMP/WATT 9.46E-021 AMP/PHOT/SEC SIG. CONDUCTANCE(1HZ)= 1.38E+001 NHOS/VATT 3.74E-020 NHOS/PHOT/SEC VOLT. RESP. (1HZ)-3.28E+010 VOLT/WATT 8.92E-011 VOLT/PHOT/SEC CURR.RESP.(1HZ)= 4.64E-901 AMP/WATT 1.26E-021 AMP/PHOT/SEC 5.75E-017 WATT/HZ11/2 NEP (IHZ)-2.11E+004 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 8.74E+011 OHMS DETECTOR BIAS-3.70E-002 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 5.43E+008 PHOTONS/SEC-CHT2 PC GAIN (Q.E.=0.3)= 2.89E-002(AC) 2.17E-001(DC)

SHOT NOISE(Q.E.=0.3)= 1.65E-006 V/HZT1/2 (AC) 4.52E-006 V/HZT1/2 (DC) BLIP NEP (Q.E.=0.3)= 5.03E-017 W/HZT1/2 (AC) 1.36E-016 W/HZT1/2 (DC)

1.72E+000 (DC)

QUAN. EFFIC. IF BLIP- 2.30E-001 (AC)

SAMPLE NO. GE:GA 4-581-1 RUN DATE 7/11/78 TEMP.=2.5 K BB INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-009 LOAD= 7.00E+010 SIG DEL V-0.91810 DC/1HZ-5
BLACKRODY CUITPUT BIAS DELTA V-0.0416 NOISE=2E-6 3.95E+907 PHOT/SEC 1.08E-013 WATTS BLACKBODY OUTPUT= SIG. CONDUCTANCE(DC)= 1.12E+882 NHOS/VATT 3.85E-819 NHOS/PHOT/SEC VOLT. RESP. (DC)= 3.87E+811 VOLT/VATT 8.36E-818 VOLT/PHOT/SEC CURR.RESP.(DC)= 4.65E+800 AMP/WATT 1.27E-820 AMP/PHOT/SEC SIG.CONDUCTANCE(1HZ)= 1.38E+801 MHOS/WATT 3.77E-828 MHOS/PHOT/SEC VOLT. RESP.(1HZ)= 4.82E+818 VOLT/WATT 1.89E-818 VOLT/PHOT/SEC CURR.RESP.(1HZ)= 5.76E-881 AMP/WATT 1.57E-821 AMP/PHOT/SEC NEP (1HZ)= 4.94E-817 WATT/HZ11/2 1.61E+884 PHOT/SEC-HZ11/ 4.94E-017 WATT/HZ11/2 1.61E+004 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 7.47E+011 OHMS DETECTOR BIAS- 4.57E-982 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= 5.86E+008 PHOTONS/SEC-CM12 PC GAIN (0.E.=0.3)= 3.59E-002(AC) 2.90E-001(DC) SHOT NOISE(Q.E.=0.3)= 2.18E-006 V/HZ11/2 (AC) 6.21E-006 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)= 5.44E-017 W/HZ11/2 (AC) 1.55E-016 W/HZ11/2 (DC) DUAN.EFFIC.IF BLIP- 3.64E-901 (AC) 2.94E+000 (DC) B8 TEMP= 58.5 BIAS=0.0600 BIAS DELTA V=0.0495
SIG DEL V=0.02100 DC/1HZ=5 NOISE=2.5E-8
BLACKBODY OUTPUT= 1.03E-013 WATTS 3.79E+007 PHOT/SEC
SIG.CONDUCTANCE(DC)= 1.13E+002 MHOS/WATT 3.06E-019 MHOS/PHOT/SEC
VOLT. RESP.(DC)= 3.65E+011 VOLT/WATT 9.90E-010 VOLT/PHOT/SEC
CURR RESP.(DC)= 5.59F+000 AMP/WATT 1.52F-020 AMP/PHOT/SEC CURR.RESP. (DC)= 5.59E+000 AMP/WATT 1.52E-020 AMP/PHOT/SEC VOLT. RESP. (1HZ)= 1.42E+901 NHOS/VATT 3.86E-929 NHOS/PHOT/SEC VOLT. RESP. (1HZ)= 4.86E+919 VOLT/VATT 1.32E-919 VOLT/PHOT/SEC CURR.RESP. (1HZ)= 7.03E-901 AMP/VATT 1.91E-921 AMP/PHOT/SEC NEP (1HZ)= 5.00E-901 AMP/VATT 1.91E-921 AMP/PHOT/SEC CURR.RESP.(1HZ)= NEP (1HZ)= 5.10E-017 WATT/HZ11/2 1.88E+004 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 6.79E+811 OHMS DETECTOR BIAS- 5.44E-002 VOLTS THE FOLLOWING ARE CALCULATED FROM ABOVE DATA PC GAIN (0.E.=0.3)= 4.37E-002(AC) 6.41E+008 PHOTONS/SEC-CMT2

SHOT NOISE(Q.E.=0.3)= 4.3/E-002(AL) 3.4/E-001(DC)
SHOT NOISE(Q.E.=0.3)= 2.73E-006 V/HZ11/2 (AC) 7.70E-006 V/HZ11/2 (DC) BLIP NEP (Q.E.=0.3)= 5.62E-017 W/HZ11/2 (AC) 1.58E-016 W/HZ11/2 (DC)

QUAN.EFFIC.IF BLIP- 3.65E-001 (AC) 2.90E+000 (DC)

3.47E-001(DC)

SAMPLE NO. GE:GA 4-5Bi-1 RUN DATE 7/11/78 TEMP .= 2.5 K BB INTEGRATED FROM 40 TO 130 MICRONS STEP 0.2 ETENDUE= 6.84E-009 LOAD= 7.80E+818

BB TEMP- 58.5 BIAS-0.0800 BIAS DELTA V-0.0620 SIG DEL V-0.82788 DC/1HZ=5.2 NOISE=5E-6 1.83E-013 WATTS BLACKBODY OUTPUT= 3.79E+007 PHOT/SEC SIG. CONDUCTANCE(DC)= 1.26E+002 NHOS/WATT 3.41E-019 NHOS/PHOT/SEC 4.59E+011 VOLT/WATT VOLT. RESP. (DC)-1.24E-009 VOLT/PHOT/SEC CURR.RESP. (DC)= 7.89E+808 AMP/WATT 2.12E-020 AMP/PHOT/SEC SIG. CONDUCTANCE(1HZ)= 1.49E+001 MHOS/WATT 4.85E-829 NHOS/PHOT/SEC 5.97E+010 VOLT/WATT 9.24E-001 AMP/WATT VOLT. RESP. (1HZ)= 1.62E-010 VOLT/PHOT/SEC CURR.RESP. (1HZ)-2.51E-021 AMP/PHOT/SEC NEP (1HZ)-8.26E-017 WATT/HZ11/2 3.84E+004 PHOT/SEC-HZ11/2 DETECTOR RESISTANCE = 4.82E+811 OHMS DETECTOR BIAS-6.81E-002 VOLTS

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= PC GAIN (Q.E.=0.3)= 5.74E-002(AC) SHOT NOISE(0.E.=0.3)= 4.28E-006 V/HZ11/2 (AC) 1.24E-006 V/HZ11/2 (DC)

BLIP NEP (Q.E.=0.3)- 7.17E-017 W/HZT1/2 (AC) 2.08E-016 W/HZT1/2 (DC) QUAN. EFFIC. IF BLIP- 2.26E-001 (AC)

88 TEMP- 58.6 BIAS-0.1880 SIG DEL V-0.82600 DC/1HZ=5.3 BLACKBODY OUTPUT= 1.84E-013 WATTS SIG. CONDUCTANCE(DC)= 1.22E+082 MHOS/WATT VOLT. RESP. (DC)-3.86E+011 VOLT/WATT CURR.RESP. (DC)= 8.19E+000 AMP/WATT SIG. CONDUCTANCE (1HZ)= 1.51E+801 MHOS/WATT VOLT. RESP. (1HZ)-5.58E+818 VOLT/WATT 1.88E+888 AMP/WATT CURR.RESP. (1HZ)= NEP (1HZ)-1.42E-016 WATT/HZ11/2 DETECTOR RESISTANCE = 1.88E+011 OHMS DETECTOR BIAS-7.29E-002 VOLTS

THE FOLLOWING ARE CALCULATED FROM ABOVE DATA BACKGROUND PHOTON FLUX DENSITY= PC GAIN (Q.E.=0.3)-8.24E-992(AC) SHOT NOISE(0.E.=0.3)= 5.77E-006 V/HZT1/2 (AC)

QUAN . EFFIC . IF BLIP-1.63E-001 (AC)

BLIP NEP (0.E.=0.3)- 1.85E-016 W/HZ11/2 (AC)

9.72E+008 PHOTONS/SEC-CHT2 4.85E-001(DC) 1.91E+000 (DC)

BIAS DELTA V-0.9663 NOISE=8E-6 3.81E+007 PHOT/SEC 3.32E-019 NHOS/PHOT/SEC 1.05E-009 VOLT/PHOT/SEC 2.28E-020 AMP/PHOT/SEC 4.11E-828 NHOS/PHOT/SEC 1.49E-010 VOLT/PHOT/SEC 2.72E-821 AMP/PHOT/SEC 5.24E+004 PHOT/SEC-HZ11/2

2.14E+009 PHOTONS/SEC-CHT2 5.84E-881(DC) 1.64E-985 V/HZT1/2 (DC) 2.98E-816 W/HZT1/2 (DC) 1.32E+000 (DC)